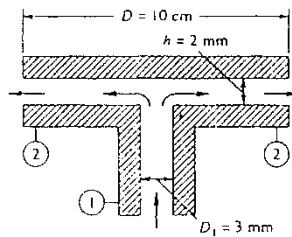


**ME:5160 (58:160) Intermediate Mechanics of Fluids**  
**Fall 2024 – HW4 Solution**

**P3.20** Oil (SG-0.91) enters the thrust bearing at 250 N/hr and exits radially through the narrow clearance between thrust plates. Compute (a) the outlet volume flow in mL/s, and (b) the average outlet velocity in cm/s.

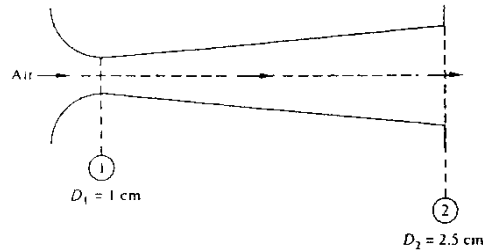


**Solution:** The specific weight of the oil is  $(0.91)(9790) = 8909 \text{ N/m}^3$ . Then

$$Q_2 = Q_1 = \frac{250/3600 \text{ N/s}}{8909 \text{ N/m}^3} = 7.8 \times 10^{-6} \frac{\text{m}^3}{\text{s}} = 7.8 \frac{\text{mL}}{\text{s}} \quad \text{Ans. (a)}$$

But also  $Q_2 = V_2 \pi (0.1 \text{ m})(0.002 \text{ m}) = 7.8 \times 10^{-6}$ , solve for  $V_2 = 1.24 \frac{\text{cm}}{\text{s}} \quad \text{Ans. (b)}$

**P3.22** The converging-diverging nozzle shown in Fig. P3.22 expands and accelerates dry air to supersonic speeds at the exit, where  $p_2 = 8$  kPa and  $T_2 = 240$  K. At the throat,  $p_1 = 284$  kPa,  $T_1 = 665$  K, and  $V_1 = 517$  m/s. For steady compressible flow of an ideal gas, estimate (a) the mass flow in kg/h, (b) the velocity  $V_2$ , and (c) the Mach number  $Ma_2$ .



**Fig. P3.22**

**Solution:** The mass flow is given by the throat conditions:

$$\dot{m} = \rho_1 A_1 V_1 = \left[ \frac{284000}{(287)(665)} \frac{\text{kg}}{\text{m}^3} \right] \frac{\pi}{4} (0.01 \text{ m})^2 \left( 517 \frac{\text{m}}{\text{s}} \right) = \mathbf{0.0604 \frac{\text{kg}}{\text{s}}} \quad \text{Ans. (a)}$$

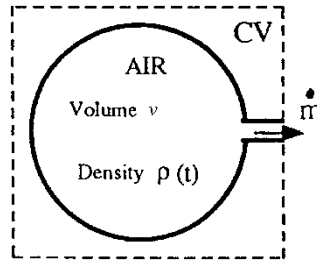
For steady flow, this must equal the mass flow at the exit:

$$0.0604 \frac{\text{kg}}{\text{s}} = \rho_2 A_2 V_2 = \left[ \frac{8000}{287(240)} \right] \frac{\pi}{4} (0.025)^2 V_2, \quad \text{or} \quad V_2 \approx \mathbf{1060 \frac{\text{m}}{\text{s}}} \quad \text{Ans. (b)}$$

Recall from Eq. (1.39) that the speed of sound of an ideal gas  $= (kRT)^{1/2}$ . Then

$$\text{Mach number at exit: } Ma = V_2/a_2 = \frac{1060}{[1.4(287)(240)]^{1/2}} \approx \mathbf{3.41} \quad \text{Ans. (c)}$$

**P3.29** In elementary compressible-flow theory (Chap. 9), compressed air will exhaust from a small hole in a tank at the mass flow rate  $\dot{m} \approx C\rho$ , where  $\rho$  is the air density in the tank and  $C$  is a constant. If  $\rho_0$  is the initial density in a tank of volume  $v$ , derive a formula for the density change  $\rho(t)$  after the hole is opened. Apply your formula to the following case: a spherical tank of diameter 50 cm, with initial pressure 300 kPa and temperature 100°C, and a hole whose initial exhaust rate is 0.01 kg/s. Find the time required for the tank density to drop by 50 percent.



**Solution:** For a control volume enclosing the tank and the exit jet, we obtain

$$0 = \frac{d}{dt} (\int \rho dv) + \dot{m}_{out}, \quad \text{or: } v \frac{d\rho}{dt} = -\dot{m}_{out} = -C\rho$$

$$\text{or: } \int_{\rho_0}^{\rho} \frac{d\rho}{\rho} = -\frac{C}{v} \int_0^t dt, \quad \text{or: } \frac{\rho}{\rho_0} \approx \exp\left[-\frac{C}{v} t\right] \quad \text{Ans.}$$

Now apply this formula to the given data. If  $p_0 = 300$  kPa and  $T_0 = 100^\circ\text{C} = 373^\circ\text{K}$ , then  $\rho_0 = p/RT = (300,000)/[287(373)] \approx 2.80$  kg/m<sup>3</sup>. This establishes the constant “C”:

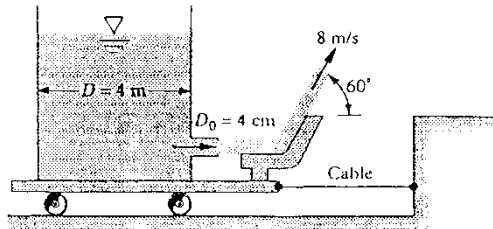
$$\dot{m}_0 = C\rho_0 = 0.01 \frac{\text{kg}}{\text{s}} = C\left(2.80 \frac{\text{kg}}{\text{m}^3}\right), \quad \text{or } C \approx 0.00357 \frac{\text{m}^3}{\text{s}} \text{ for this hole.}$$

The tank volume is  $v = (\pi/6)D^3 = (\pi/6)(0.5 \text{ m})^3 \approx 0.0654$  m<sup>3</sup>. Then we require

$$\rho/\rho_0 = 0.5 = \exp\left[-\frac{0.00357}{0.0654} t\right] \quad \text{if } t \approx 13 \text{ s} \quad \text{Ans.}$$

**P3.58** The water tank in Fig. P3.58 stands on a frictionless cart and feeds a jet of diameter 4 cm and velocity 8 m/s, which is deflected 60° by a vane. Compute the tension in the supporting cable.

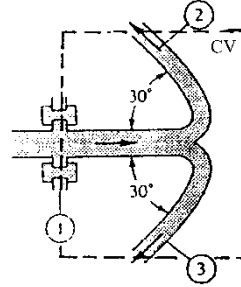
**Solution:** The CV should surround the tank and wheels and cut through the cable and the exit water jet. Then the horizontal force balance is



**Fig. P3.58**

$$\sum F_x = T_{\text{cable}} = \dot{m}_{\text{out}} u_{\text{out}} = (\rho A V_j) V_j \cos \theta = 998 \left( \frac{\pi}{4} \right) (0.04)^2 (8)^2 \cos 60^\circ = 40\text{ N} \quad \text{Ans.}$$

**P3.62** Water at 20°C exits to the standard sea-level atmosphere through the split nozzle in Fig. P3.62. Duct areas are  $A_1 = 0.02 \text{ m}^2$  and  $A_2 = A_3 = 0.008 \text{ m}^2$ . If  $p_1 = 135 \text{ kPa}$  (absolute) and the flow rate is  $Q_2 = Q_3 = 275 \text{ m}^3/\text{h}$ , compute the force on the flange bolts at section 1



**Solution:** With the known flow rates, we can compute the various velocities:

$$V_2 = V_3 = \frac{275/3600 \text{ m}^3/\text{s}}{0.008 \text{ m}^2} = 9.55 \frac{\text{m}}{\text{s}}; \quad V_1 = \frac{550/3600}{0.02} = 7.64 \frac{\text{m}}{\text{s}}$$

The CV encloses the split nozzle and cuts through the flange. The balance of forces is

$$\sum F_x = -F_{\text{bolts}} + p_{1,\text{gage}} A_1 = \rho Q_2 (-V_2 \cos 30^\circ) + \rho Q_3 (-V_3 \cos 30^\circ) - \rho Q_1 (+V_1),$$

$$\begin{aligned} \text{or: } F_{\text{bolts}} &= 2(998) \left( \frac{275}{3600} \right) (9.55 \cos 30^\circ) + 998 \left( \frac{550}{3600} \right) (7.64) + (135000 - 101350)(0.02) \\ &= 1261 + 1165 + 673 \sim \mathbf{3100N \text{ Ans.}} \end{aligned}$$