

Problem 2:

From Problem 1,

$$\begin{aligned}\sigma_1 &= \frac{K_I}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \left[1 + \sin \frac{\theta}{2} \right] \\ \sigma_2 &= \frac{K_I}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \left[1 - \sin \frac{\theta}{2} \right] \\ \sigma_3 &= \begin{cases} 0, & \text{plane stress} \\ \nu(\sigma_1 + \sigma_2), & \text{plane strain} \end{cases}\end{aligned}\quad . \quad (10)$$

(a) Expressions of Plastic Zone Boundary (Mode-I; Tresca)

Plane Stress

The maximum shear stress τ_{\max} is (Note, $\sigma_1 \geq \sigma_2 \geq \sigma_3$ for $0 \leq \theta \leq \pi$)

$$\tau_{\max} = \frac{\sigma_1 - \sigma_3}{2} = \frac{1}{2} \frac{K_I}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \left[1 + \sin \frac{\theta}{2} \right]. \quad (11)$$

Hence, the Tresca yield criterion becomes

$$\tau_{\max}|_{r=r_y} = \frac{S_y}{2}, \quad (12)$$

i.e.,

$$\frac{1}{2} \frac{K_I}{\sqrt{2\pi r_y}} \cos \frac{\theta}{2} \left[1 + \sin \frac{\theta}{2} \right] = \frac{S_y}{2}, \quad (13)$$

which can be solved to obtain

$$\boxed{r_y(\theta) = \frac{K_I^2}{2\pi S_y^2} \cos^2 \frac{\theta}{2} \left[1 + \sin \frac{\theta}{2} \right]^2, \quad 0 \leq |\theta| \leq \pi.} \quad (14)$$

Note, Equation 14 is also valid for $-\pi \leq \theta \leq 0$, as the plastic zone is symmetrical w.r.t. crack (horizontal axis) line.

Plane Strain

To obtain τ_{\max} , ordering of principal stresses is important. For $0 \leq \theta \leq \pi$ and $0 \leq \nu \leq 0.5$, σ_1 is always the largest. However, for σ_2 and σ_3 , there are two possibilities, i.e.,

$$\sigma_1 \geq \sigma_2 \geq \sigma_3 \quad \text{or} \quad \sigma_1 \geq \sigma_3 \geq \sigma_2,$$

depending on the value of the Poisson's ratio. Hence,

$$\tau_{\max} = \begin{cases} \frac{\sigma_1 - \sigma_3}{2} = \frac{\sigma_1(1-\nu) - \nu\sigma_2}{2}, & \text{if } \sigma_1 \geq \sigma_2 \geq \sigma_3 \\ \frac{\sigma_1 - \sigma_2}{2}, & \text{if } \sigma_1 \geq \sigma_3 \geq \sigma_2 \end{cases}. \quad (15)$$

The Tresca yield criterion is

$$\tau_{\max} = \begin{cases} \frac{\sigma_1 - \sigma_3}{2} = \frac{\sigma_1(1-\nu) - \nu\sigma_2}{2}, & \text{if } \sigma_1 \geq \sigma_2 \geq \sigma_3 \\ \frac{\sigma_1 - \sigma_2}{2}, & \text{if } \sigma_1 \geq \sigma_3 \geq \sigma_2 \end{cases} = \frac{S_y}{2}. \quad (16)$$

which can be solved to obtain

$$r_y(\theta) = \begin{cases} \frac{K_I^2}{2\pi S_y^2} \cos^2 \frac{\theta}{2} \left[(1-2\nu) + \sin \frac{\theta}{2} \right]^2, & \text{if } \sigma_1 \geq \sigma_2 \geq \sigma_3 \\ \frac{K_I^2}{2\pi S_y^2} \sin^2 \theta, & \text{if } \sigma_1 \geq \sigma_3 \geq \sigma_2 \end{cases}. \quad (17)$$

or,

$$r_y(\theta) = \frac{K_I^2}{\pi S_y^2} \times \frac{1}{2} \max \left\{ \cos^2 \frac{\theta}{2} \left[(1-2\nu) + \sin \frac{\theta}{2} \right]^2, \sin^2 \theta \right\}, \quad 0 \leq |\theta| \leq \pi. \quad (18)$$

Note, Equation 14 is also valid for $-\pi \leq \theta \leq 0$, as the plastic zone is symmetrical w.r.t. crack (horizontal axis) line.