# THE UNIVERSITY OF IOWA Department of Mechanical Engineering 

## Fracture Mechanics <br> ME:5159

Homework \#2
Total Points: 20

Assigned: February 17, 2020
Due: February 28, 2020

## Problem 1:

A linear-elastic finite element analysis is performed for a wide (infinite) plate with a through crack (see figure below) subjected to mode-I tensile loading. The far-field tensile stress is $\sigma^{\infty}=200 \mathrm{MPa}$ and the crack length is $2 a=50 \mathrm{~mm}$. Assuming plane strain condition, the stress normal to the crack plane $\left(\sigma_{y}\right)$ at $\theta=0$ and relative displacement $\left(u_{y}\right)$ at $\theta=\pi$ are calculated at node points near the crack tip as a function of $r / a$ and are tabulated below. The elastic constants are as follows: $E=192 \mathrm{GPa}$ and $v=0.2$.


| $\theta=0$ |  | $\theta=\pi$ |  |
| :---: | :---: | :---: | :---: |
| $r / a$ | $\sigma_{y} / \sigma^{\infty}$ | $r / a$ | $u_{y} / 2 a$ |
| 0.005 | 11 | 0.005 | $9.99 \times 10^{-5}$ |
| 0.01 | 8.07 | 0.01 | $1.41 \times 10^{-4}$ |
| 0.02 | 6 | 0.02 | $1.99 \times 10^{-4}$ |
| 0.04 | 4.54 | 0.04 | $2.80 \times 10^{-4}$ |
| 0.06 | 3.89 | 0.06 | $3.41 \times 10^{-4}$ |
| 0.08 | 3.5 | 0.08 | $3.92 \times 10^{-4}$ |
| 0.1 | 3.24 | 0.1 | $4.36 \times 10^{-4}$ |
| 0.15 | 2.83 | 0.15 | $5.27 \times 10^{-4}$ |
| 0.2 | 2.58 | 0.2 | $6.00 \times 10^{-4}$ |
| 0.25 | 2.41 | 0.25 | $6.61 \times 10^{-4}$ |

Using the correlation methods, one can estimate the mode-I stress-intensity factor (SIF) for this problem from the following equations:

## Stress-Correlation Method (Equation 4 in Lecture No. 9)

$$
\begin{equation*}
\sigma_{y}=\frac{K_{I}}{\sqrt{2 \pi r}} \quad(\text { for } \theta=0) \tag{1}
\end{equation*}
$$

## Displacement-Correlation Method (Equation 3 in Lecture No. 12)

$$
\begin{equation*}
u_{y}=\frac{K_{I}}{\mu} \sqrt{\frac{r}{2 \pi}}(2-2 v) \quad(\text { for } \theta=\pi) \tag{2}
\end{equation*}
$$

1. Using Equations 1 and 2 and the tabulated finite element results of $\sigma_{y}$ and $u_{y}$, estimate the SIFs as a function of $r / a$, and denote them as $K_{I, S C}$ and $K_{I, D C}$, respectively.
2. Recall that the exact solution $\left(K_{I, E}\right)$ of SIF for this problem is (Equation 5 in Lecture No. 9)

$$
\begin{equation*}
K_{I, E}=\sigma^{\infty} \sqrt{\pi a} \tag{3}
\end{equation*}
$$

To evaluate the accuracy of stress- and displacement-correlation methods, define two error functions, such as,

$$
\begin{equation*}
e_{S C}=\frac{K_{I, E}-K_{I, S C}}{K_{I, E}} \times 100 \tag{4}
\end{equation*}
$$

and

$$
\begin{equation*}
e_{D C}=\frac{K_{I, E}-K_{I, D C}}{K_{I, E}} \times 100, \tag{5}
\end{equation*}
$$

respectively. Develop plots of $e_{S C}$ and $e_{D C}$ as a function of $r / a$. Which correlation method gives better accuracy? Why? Comments.

## Problem 2:

Consider a material which has $K_{\text {Ic }}=40 \mathrm{MPa} \sqrt{\mathrm{m}}(36.4 \mathrm{ksi} \sqrt{ } \mathrm{in})$. Each of the five specimens in Table on page 81 of Lecture No. 10 has been fabricated from this material. Assume: $B=25.4 \mathrm{~mm}(1 \mathrm{inch}), W$ $=50.8 \mathrm{~mm}$ ( 2 inches), $S / W=4$, and $a / W=0.5$. If failure occurs when $K_{I}>K_{I c}$, estimate the failure load for each specimen. Which specimen has the highest failure load? Which has the lowest? Comments.

