

**November 19, 2014**

1. Kerosene at  $20^\circ\text{C}$  ( $\gamma = 50.2 \text{ lbf/ft}^3$ ) flows through the pump in Fig. 2 at  $2.3 \text{ ft}^3/\text{s}$ . The total head loss between sections 1 and 2 is  $h_L = 8 \text{ ft}$  and the mercury manometer reading is  $h = 4 \text{ ft}$ . Find (a) the velocities  $V_1$  and  $V_2$ , (b) the pressure rise  $\Delta p = p_2 - p_1$  across the pump and (c) the power  $\dot{W}_p$  delivered by the pump. (Note:  $1 \text{ hp} = 550 \text{ ft}\cdot\text{lbf/s}$ )

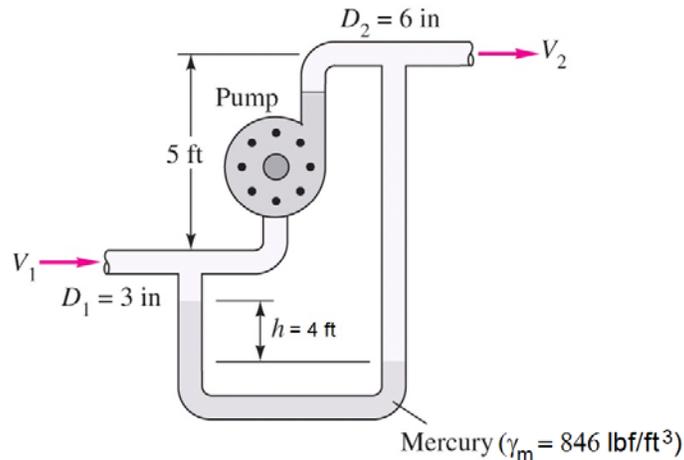


Figure 1

2. Water ( $\gamma = 62.4 \text{ lb/m}^3$  and  $\rho = 1.94 \text{ slugs/ft}^3$ ) flows steadily in a pipe and exits to the atmosphere as a free jet through a nozzle-end that contains a filter as shown in Fig. 1. If the head loss  $h_L$  for the flow through the nozzle-end is  $2.5 \text{ ft}$ , determine (a) the pressure at the section (1) and (b) the axial component  $R_x$  of the anchoring force needed to keep the nozzle stationary. The flow is in a *horizontal* plane such that the sections (1) and (2) are at the same elevation in the vertical plane and the weight of the nozzle and the water in it does *not* contribute to the anchoring force.

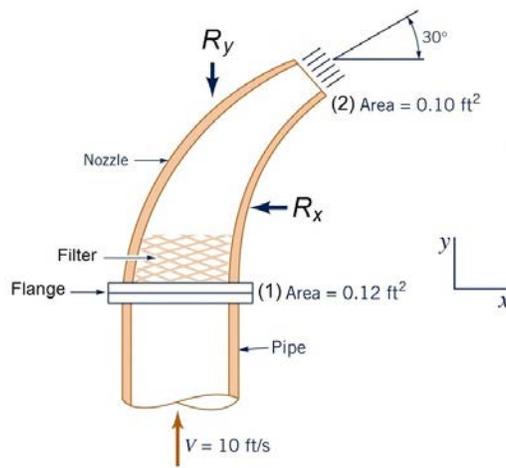


Figure 2

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3. A useful approximation for the  $x$  component of velocity in a steady incompressible viscous laminar flow between two stationary parallel flat plates in Fig. 3 is

$$\frac{d^2u}{dy^2} = -\frac{1}{\mu} \left( \frac{\Delta p}{L} \right)$$

where,  $\mu$  is the fluid viscosity and  $\Delta p = p_{\text{out}} - p_{\text{in}}$  is the pressure drop along the plate length  $L$ . (a) By integrating the given equation then applying appropriate boundary conditions, derive an expression for the velocity distribution  $u(y)$ . (b) If the fluid is SAE 30 oil at  $15.6^\circ\text{C}$  ( $\mu = 3.8 \times 10^{-1} \text{ N}\cdot\text{s}/\text{m}^2$ ),  $h = 2.5 \text{ mm}$ ,  $L = 1.5 \text{ m}$ ,  $W = 0.75 \text{ m}$ ,  $p_{\text{in}} = 101.3 \text{ kPa}$ , and  $p_{\text{out}} = 0$ , estimate the wall shear stress  $\tau_w$  and the shearing force  $F_s$  acting on the *bottom* plate.

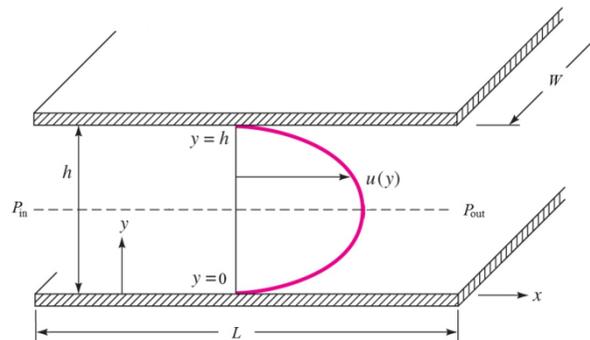


Figure 3

4. Heat exchangers often consist of many triangular passages. Typical is Fig. 4 with length  $L$  and side length  $b$ . Under laminar conditions, the volume flow  $Q$  through the tube is a function of viscosity  $\mu$ , pressure drop per unit length  $\Delta p_L$ , and  $b$  such that  $Q = f(\mu, \Delta p_L, b)$ . (a) Using the Buckingham pi theorem, find a suitable pi parameter  $\Pi$  for this problem. (b) For one pi parameter the functional relationship must be  $\Pi = C$ , where  $C$  is a constant. Determine by what factor the volume flow will change if the side length  $b$  of the tube is doubled.

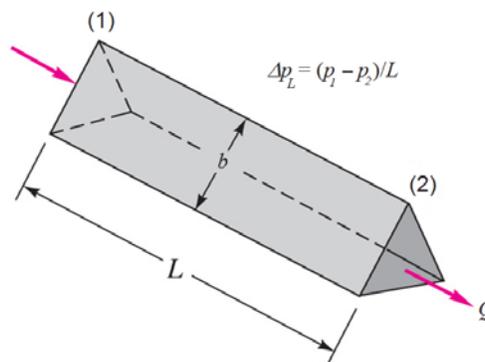


Figure 4