# **EXAM1 Solutions**

Problem 1: Shear stress (Chapter 1) Information and assumptions

- $v = 1.28 \times 10^{-2} ft^2/s$
- $\rho_{water} = 1.94 \, slugs/ft^3$
- SG = 1.26
- $u(y) = \frac{B}{2\mu}(y^2 hy) + V\left(1 \frac{y}{b}\right)$
- V = 0.02 ft/s
- *h* = 1.0 *in*
- $B = -0.334 \ lb/ft^3$
- $A = 100 f t^2$



Find

• Find (a) shear stress on the plate, (b) required force, and (c) power to pull the plate

### **Solution**

(a) Calculate dynamic viscosity

$$\mu = \nu \cdot \rho = \nu \cdot (SG \cdot \rho_{water}) = (1.28 \times 10^{-2})(1.26 \times 1.94) = 3.13 \times 10^{-2} \text{ lb} \cdot \text{s/ft}^2 + 1$$

Shear stress

$$\tau = \mu \frac{du}{dy} + 5$$
$$\tau = \mu \left(\frac{B}{2\mu}(2y - h) - \frac{V}{b}\right) + 1$$

Shear stress at the wall (at y=0)

$$\therefore \tau = (3.13 \times 10^{-2}) \left( \frac{(-0.334)}{(2)(3.13 \times 10^{-2})} \left( 2 \times 0 - \frac{1}{12} \right) - \frac{(0.02)}{(1/12)} \right) = \mathbf{0.0064} \ \mathbf{lb/ft^2} + 1$$

(b) Friction force

$$F = \tau \cdot A = (0.0064)(100) = 0.64 \, \text{lb} + 1$$

(c) Power

$$P = F \cdot V = (0.64)(0.02) = 0.0128 \text{ lb} \cdot \text{ft/s} + 1$$

1.131

**11.1(31** (See Fluids in the News article titled "Walking on water," Section 1.9.) (a) The water strider bug shown in Fig. P1.)31 is supported on the surface of a pond by surface tension acting along the interface between the water and the bug's legs. Determine the minimum length of this interface needed to support the bug. Assume the bug weighs  $10^{-4}$  N and the surface tension force acts vertically upwards. (b) Repeat part (a) if surface tension were to support a person weighing 750 N.



FIGURE PI.13



(b) 
$$l = \frac{750 \text{ N}}{7.34 \times 10^{-2} \text{ N}} = \frac{1.02 \times 10^{4} \text{ m}}{1000 \text{ m}} (6.34 \text{ mi})$$

2. 4.3 Water 2.312 For the inclined-tube manometer of Fig. P2.43 the pressure in pipe A is 0.6 psi. The fluid in both pipes A and B is water, and the gage fluid in the manometer has a specific Water gravity of 2.6. What is the pressure in pipe B corresponding to the differential reading shown? SG = 2.63 in. FIGURE P2.43  $P_A + \delta_{H_0} \left(\frac{3}{12}f_t\right) - \delta_{gf} \left(\frac{8}{12}f_t\right) \sin 30^\circ - \delta_{H_0} \left(\frac{3}{12}f_t\right) = P_3$ (where def is the specific weight of the gage fluid) Thus, PB = PA - dgf ( = ft) sin 300  $= \left(0, 6 \frac{15}{10.2}\right) \left(144 \frac{10.7}{5t^2}\right) - (2.6)(62, 4 \frac{15}{5t^3}) \left(\frac{8}{12} ft\right) (0.5) = 32.3 \frac{16}{5t^3}$ =  $32.3 \frac{15}{5t^2} \frac{1}{144} \frac{10.7}{12} \frac{1}{5t^2} = 0.224 \frac{1}{55}$ 2.44 2.44 A flowrate measuring device is installed in a horizontal pipe through which water is flowing. A U-tube manometer is connected to the pipe through pressure taps located 3 in. on either side of the device. The gage fluid in the manometer has a specific weight of 112 lb/ft3. Determine the differential reading of the manometer corresponding to a pressure drop between the taps of 0.5 lb/in.<sup>2</sup>. flowmeter flow (water) \$ 8420 Dat Let p, and p2 be pressures at pressure taps. Write manometer equation between p, and p2. Thus Il wall of  $p_1 + \delta_{H_20}(h_1 + h) - \delta_{gf}h - \delta_{H_20}h_1 = p_2$ so that  $h = \frac{p_1 - p_2}{\delta_{qf} - \delta_{H_{20}}} = \frac{\left(0.5 \frac{lb}{ln_2}\right) \left(144 \frac{ln^2}{ft^2}\right)}{112 \frac{lb}{ft^3} - 62.4 \frac{lb}{ft^3}}$ = <u>1.45 ft</u> 2-:40

## September 16, 2013

NAME

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Quiz 2.

A large, open tank contains water and is connected to a 6-ft-diameter conduit as shown the Figure. A circular plug is used to seal the conduit. (Hints:  $I_{xc} = \pi R^4/4$ ,  $\gamma = 62.4 \text{ lb/ft}^3$ )

(a) Determine the magnitude of the force of the water  $(F_R)$  on the plug. (+4 points)

(b) Determine the location  $(y_R)$  and direction of the force of the water on the plug. (+3 points)

Note: Attendance (+2 points), Format (+1 points)

Solution:

a)

$$F_R = p_c \cdot A \tag{+2 points}$$

$$p_c = \gamma \cdot h_c$$
, where  $h_c = 12 ft$  (+1 point)

$$A = \frac{\pi D^2}{4}$$
(+0.5 point)

$$F_R = \left(62.4 \ \frac{lb}{ft^3}\right) (12 \ ft) \left(\frac{\pi (6 \ ft)^2}{4}\right) = 21,200 \ lb \tag{+0.5 point}$$

b)

$$y_{R} = y_{c} + \frac{I_{xc}}{y_{c} \cdot A}$$
(+2 points)  

$$I_{xc} = \frac{\pi R^{4}}{4} = \frac{\pi (3ft)^{4}}{4} = 63.6 ft^{4}$$
  

$$y_{R} = 12 ft + \frac{63.6 ft^{4}}{(12 ft)\pi (3 ft)^{2}} = 12.19 ft$$
(+0.5 point)

The force acts below the water surface and is perpendicular to the plug surface as shown in the Figure below.

(+0.5 point)





2.82

**2.82** A structure is attached to the ocean floor as shown in Fig. P2.82 A 2-m-diameter hatch is located in an inclined wall and hinged on one edge. Determine the minimum air pressure,  $p_1$ ,  $\tilde{T}$  Seawate within the container to open the hatch. Neglect the weight of the hatch and friction in the hinge.







To locate 
$$F_R$$
,  
 $y_R = \frac{T_{xc}}{y_c A} + y_c$  where  $y_c = \frac{10 m}{sin 30^\circ} + 1m = 21 m$ 

So that  

$$y_{R} = \frac{\left(\frac{\pi}{4}\right)(lm)^{4}}{(2lm)(\pi)(1m)^{2}} + 2lm = 2l.012m$$

For equilibrium,  

$$\Sigma M_{\mu} = 0$$

50 that

and

$$F_{R}(21.012m - 20m) = p_{1}(TT)(1m)^{2}(1m)$$

$$P_{l} = \frac{(3.33 \times 10^{5} N)(1.012 m)}{\pi (1m)^{2}(1m)} = \frac{107 k P_{a}}{107 k P_{a}}$$



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Quiz 3. The quarter circle gate BC in Figure 1 is hinged at *C*. Find the horizontal force *P* required to hold the gate stationary. The gate width into the paper is 3 m. Neglect the weight of the gate.

Resources:

- $F_H = \bar{p}A_{proj};$   $F_V = \gamma \Psi$   $y_{cp} = \bar{y} + I_{xc}/\bar{y}A_{proj};$   $x_{cp} = \bar{x}$  of  $\Psi$
- $\gamma = 9,780 N/m^3$  for water







Note: Attendance (+2 points), Format (+1 points) Solution:

The horizontal component of water force is

$$F_H = \gamma h_c A_{proj} = \left(9790 \frac{N}{m^3}\right) (1 \ m) (2 \times 3 \ m^2) = 58,740 \ N \tag{+2 points}$$

and the vertical component of water force is

$$F_V = \gamma \Psi = \left(9790 \frac{N}{m^3}\right) \left[ \left(\frac{\pi}{4}\right) (2 \ m)^2 (3 \ m) \right] = 92,270 \ N \tag{+2 points}$$

The pressure center is

$$x_{cp} = \frac{4R}{3\pi} = \frac{(4)(2\ m)}{3\pi} = 0.849\ m \tag{+1 point}$$

$$y_{cp} = \bar{y} + \frac{I_{xc}}{\bar{y}A_{proj}} = (1\ m) + \frac{(3\ m)(2\ m)^3/12}{(1\ m)(2\ m)(3\ m)} = 1.333\ m \tag{+1 point}$$

where  $x_{cp}$  is from the left of C and  $y_{cp}$  is down from the surface. Sum moments clockwise about point C:

$$\sum M_C = 0 = P \times (2m) - (58,740 N)(2m - 1.333 m) - (92,270 N)(0.849 m)$$

$$P = 58,700 N = 58.7 kN$$
(+1 point)

3.51

**3.51** Water flows through the pipe contraction shown in Fig. P3.51. For the given 0.2-m difference in the manometer level, determine the flowrate as a function of the diameter of the small pipe, D.



$$\begin{split} \frac{\mathcal{A}_{i}}{\mathcal{B}} + \frac{\mathcal{V}_{i}^{2}}{2g} + \mathbb{Z}_{i} &= \frac{\mathcal{P}_{2}}{\mathcal{B}} + \frac{\mathcal{V}_{2}^{2}}{2g} + \mathbb{Z}_{2} & \text{with } \mathcal{A}_{i}\mathcal{V}_{i} = \mathcal{A}_{2}\mathcal{V}_{2} \\ \text{Thus, with } \mathbb{Z}_{i} = \mathbb{Z}_{2} & \text{or } \mathcal{V}_{2} = \frac{\left(\frac{\pi}{\mathcal{P}} D_{i}^{2}\right)}{\left(\frac{\pi}{\mathcal{P}} D_{2}^{2}\right)} \mathcal{V}_{i} = \left(\frac{0.1}{D}\right)^{2} \mathcal{V}_{i} \\ \frac{\mathcal{P}_{i} - \mathcal{P}_{2}}{\mathcal{B}} &= \frac{\mathcal{V}_{2}^{2} - \mathcal{V}_{i}^{2}}{2g} = \frac{\left[\left(\frac{0.1}{D}\right)^{4} - 1\right] \mathcal{V}_{i}^{2}}{2g} \\ \frac{\mathcal{D}_{i}\mathcal{H}}{\mathcal{P}_{i}} = \delta h_{i} & and \quad \mathcal{P}_{2} = \delta h_{2} \quad so \quad that \quad \mathcal{P}_{i} - \mathcal{P}_{2} = \delta'(h_{i} - h_{2}) = 0.2 \,\delta' \\ \frac{\mathcal{D}_{i}\mathcal{B}}{\mathcal{B}} &= \frac{\left[\left(\frac{0.1}{D}\right)^{4} - 1\right] \mathcal{V}_{i}^{2}}{2g} & \text{or } \mathcal{V}_{i} = \sqrt{\frac{0.2 \left(2g\right)}{\left[\left(\frac{0.1}{D}\right)^{4} - 1\right]}} \\ and \\ \mathcal{Q} = \mathcal{A}_{i}\mathcal{V}_{i} = \frac{\pi}{4} \left(0.1\right)^{2} \sqrt{\frac{0.2 \left(2 \left(9.81\right)\right)}{\left[\left(\frac{0.1}{D}\right)^{4} - 1\right]}} \end{split}$$

or

$$Q = \frac{0.0156 D^2}{\sqrt{(0.1)^4 - D^4}} \frac{m^3}{s} \text{ when } D \sim m$$

3-44

September 30, 2016

### NAME

Quiz 5. When a valve is opened, fluid flows in the expansion duct shown below according to the approximation

$$\underline{V} = u\hat{\imath} = U\left(1 - \frac{x}{2L}\right)\left(\frac{Ut}{L}\right)\hat{\imath}$$

for t  $\ll L/U$ . If L = 1 m and U = 1 m/s, then at (x, t) = (L, L/2U),

1) Find the unsteady (local) acceleration of  $a_x$ 

2) Find the convective acceleration of  $a_x$ 

3) Find the total acceleration  $a_x$ 



Acceleration:  $a_{x} = \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z}$   $a_{y} = \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z}$   $a_{z} = \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z}$ 

Note: Attendance (+2 points), format (+1 point) Solution:

1) local acceleration

$$(a_x)_{local} = \frac{\partial u}{\partial t} = \frac{\partial}{\partial t} \left[ U \left( 1 - \frac{x}{2L} \right) \left( \frac{Ut}{L} \right) \right] = \frac{U^2}{L} \left( 1 - \frac{x}{2L} \right)$$
(+2 points)

at (x, t) = (L, L/2U),

$$(a_x)_{local} = \frac{U^2}{L} \left( 1 - \frac{L}{2L} \right) = \frac{U^2}{2L} = \frac{(1 \text{ m/s})^2}{2 \times 1 \text{ m}} = 0.5 \frac{\text{m}}{\text{s}^2}$$
(+1 points)

2) convective acceleration

$$(a_x)_{conv} = u \frac{\partial u}{\partial x} = U \left( 1 - \frac{x}{2L} \right) \left( \frac{Ut}{L} \right) \frac{\partial}{\partial x} \left[ U \left( 1 - \frac{x}{2L} \right) \left( \frac{Ut}{L} \right) \right] = -\frac{U^2}{2L} \left( 1 - \frac{x}{2L} \right) \left( \frac{Ut}{L} \right)^2$$
(+2 points)

at (x, t) = (L, L/2U),

$$(a_x)_{conv} = -\frac{U^2}{2L} \left(1 - \frac{L}{2L}\right) \left(\frac{U}{L} \cdot \frac{L}{2U}\right)^2 = -\frac{U^2}{16L} = -\frac{(1 \text{ m/s})^2}{16 \times 1 \text{ m}} = -0.0625 \frac{\text{m}}{\text{s}^2}$$
(+1 points)

## September 30, 2016

3) total acceleration

$$a_x = (a_x)_{local} + (a_x)_{conv} = \frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} = \frac{U^2}{2L}\left(1 - \frac{x}{2L}\right)\left(1 - \frac{1}{2}\left(\frac{Ut}{L}\right)^2\right)$$
(+0.5 points)

at (x, t) = (L, L/2U),

$$a_x = \frac{U^2}{L} \left( 1 - \frac{L}{2L} \right) \left( 1 - \frac{1}{2} \left( \frac{U}{L} \cdot \frac{L}{2U} \right)^2 \right) = \frac{7U^2}{16L} = \frac{7 \times (1 \text{ m/s})^2}{16 \times 1 \text{ m}} = 0.4375 \frac{\text{m}}{\text{s}^2}$$
(+0.5 points)