

- 2.1 (a) By an energy balance, the bicycle stops when final potential energy equals initial kinetic energy. Therefore

$$\frac{1}{2}mv_i^2 = mgh_f \quad \text{or} \quad h_f = \frac{v_i^2}{2g} = \frac{\left(20 \frac{\text{km}}{\text{hr}} \times 1000 \frac{\text{m}}{\text{km}} \times \frac{1 \text{ hr}}{3600 \text{ sec}}\right)^2}{2 \times 9.807 \frac{\text{m}}{\text{sec}^2}}$$

or $h=1.57 \text{ m}$.

- (b) The energy balance now is

$$\frac{1}{2}mv_f^2 = \frac{1}{2}mv_i^2 + mgh_i \quad \text{or} \quad v_f^2 = v_i^2 + 2gh_i$$

$$v_f^2 = \left(20 \frac{\text{km}}{\text{hr}}\right)^2 + 2 \times 9.807 \frac{\text{m}}{\text{sec}^2} \times 70 \text{ m} \times \left(\frac{\text{km}}{1000 \text{ m}} \times \frac{3600 \text{ sec}}{\text{hr}}\right)^2$$

$v_f = 134.88 \text{ km/hr}$. Anyone who has bicycled realizes that this number is much too high, which demonstrates the importance of air and wind resistance.

- 2.2 The velocity change due to the 55 m fall is

$$(\Delta v^2) = 2 \times 9.807 \frac{\text{m}}{\text{sec}^2} \times 55 \text{ m} \times \left(\frac{\text{km}}{1000 \text{ m}} \times \frac{3600 \text{ sec}}{\text{hr}}\right)^2$$

$v_f = 118.24 \text{ km/hr}$. Now this velocity component is in the vertical direction. The initial velocity of 8 km/hr was obviously in the horizontal direction. So the final velocity is

$$v = \sqrt{v_x^2 + v_y^2} = 118.51 \frac{\text{km}}{\text{hr}}$$

- 2.3 (a) System: contents of the piston and cylinder
(closed isobaric = constant pressure)

$$\text{M.B.: } M_2 - M_1 = \Delta M = 0 \Rightarrow M_2 = M_1 = M$$

$$\text{E.B.: } M_2 \hat{U}_2 - M_1 \hat{U}_1 = \Delta M \left(\hat{H} \right)^0 + Q + \cancel{W_s}^0 - \int P dV$$

$$M(\hat{U}_2 - \hat{U}_1) = Q - \int P dV = Q - P \int dV = Q - P(V_2 - V_1)$$

$$M(\hat{U}_2 - \hat{U}_1) = Q - PM(\hat{V}_2 - \hat{V}_1)$$

$$\begin{aligned} Q &= M(\hat{U}_2 - \hat{U}_1) + M(P\hat{V}_2 - P\hat{V}_1) = M[(\hat{U}_2 + P\hat{V}_2) - (\hat{U}_1 + P\hat{V}_1)] \\ &= M(\hat{H}_2 - \hat{H}_1) \end{aligned}$$

$$P = 1.013 \text{ bar} \approx 0.1 \text{ MPa}$$

	\hat{V}	\hat{U}	\hat{H}	
$T = 100$	1.6958	2506.7	2676.2	
$T = 150$	1.9364	2582.8	2776.4	
Linear interpolation				
$T = 125^\circ\text{C}$	1.8161	2544.8	2726.3	Initial state
Final state	$P = 0.1 \text{ MPa}, \hat{V}_2 = 3.6322 \text{ m}^3/\text{kg}$			
$T = 500^\circ\text{C}$	3.565		3488.1	
$T = 600^\circ\text{C}$	4.028		3704.7	
Linear interpolation				

$$\frac{3.6322 - 3.565}{4.028 - 3.565} = \frac{T_2 - 500}{600 - 500} \quad T_2 = 514.5^\circ\text{C}$$

$$\frac{514.5 - 500}{600 - 500} = \frac{\hat{H}_2 - 3488.1}{3704.7 - 3488.1} \quad \hat{H}_2 = 3519.5$$

$$Q = 1 \text{ kg}(3519.5 - 2726.3) \text{ kJ/kg} = 793.2 \text{ kJ}$$

$$\begin{aligned} W &= -\int P dV = -1 \text{ bar} \times (V_2 - V_1) = -1 \text{ bar} \times (3.6322 - 1.8161) \text{ m}^3/\text{kg} \\ &= -1 \text{ bar} \times 100,000 \frac{\text{Pa}}{\text{bar}} \times \frac{1 \text{ kg}}{\text{m} \cdot \text{s}^2 \cdot \text{Pa}} \times \frac{1 \text{ J}}{\text{m}^2 \cdot \text{s}^2 \cdot \text{kg}} \times 1.8161 \text{ m}^3/\text{kg} \\ &= -181.6 \text{ kJ/kg} \end{aligned}$$

(b) System is closed and constant volume

$$\text{M.B.: } M_2 = M_1 = M$$

$$\begin{aligned} \text{E.B.: } M_2 \hat{U}_2 - M_1 \hat{U}_1 &= \cancel{\Delta M (\hat{H})}^0 + Q + \cancel{W_s}^0 - \cancel{\int P dV}^0 \\ Q &= M(\hat{U}_2 - \hat{U}_1) \end{aligned}$$

Here final state is $P = 2 \times 1.013 \text{ bar} \sim 0.2 \text{ MPa}$; $\hat{V}_2 = \hat{V}_1 = 1.8161 \text{ m}^3/\text{kg}$
(since piston-cylinder volume is fixed)

$$P = 0.2 \text{ MPa}; \hat{V}_2 = 1.8161$$

$T(^{\circ}\text{C})$	\hat{V}	\hat{U}
500	1.7814	3130.8
600	2.013	3301.4

$$\frac{1.8161 - 1.7814}{2.013 - 1.7814} = \frac{T - 500}{600 - 500} = \frac{0.0347}{0.2316} = 0.1498 \sim 0.15$$

$$T = 515^\circ\text{C}$$

$$\begin{aligned} \frac{\hat{U}_2 - 3130.8}{3301.4 - 3130.8} &= 0.1498 \quad \hat{U}_2 = 3156.4 \text{ kJ/kg} \\ Q &= 1 \text{ kg} \times (3156.4 - 2544.8) \text{ kJ/kg} = 611.6 \text{ kJ} \end{aligned}$$

(c) Steam as an ideal gas—constant pressure

$$N = \frac{PV}{RT} \Rightarrow \frac{P_1 V_1}{RT_1} = \frac{P_2 V_2}{RT_2} \text{ but } V_2 = 2V_1; P_1 = P_2$$

$$\frac{P_1 \underline{V}_1}{T_1} = \frac{P_2 \underline{V}_2}{T_2} \Rightarrow T_2 = 2 \times T_1$$

$$T_1 = 273.15 + 125 = 398.15 \text{ K}$$

$$T_2 = 2 \times T_1 = 796.3 \text{ K} = 523.15^\circ \text{C}$$

$$Q = N \Delta \underline{H} = \frac{1000 \text{ g/kg}}{18 \text{ g/mol}} \times 34.4 \text{ J/mol K} \times (796.3 - 398.15) \text{ K} \times \frac{1 \text{ kJ}}{1000 \text{ J}}$$

$$= 760.9 \text{ kJ}$$

$$W = -\int P dV = -P \Delta V = -P \left(\frac{NRT_2}{P} - \frac{NRT_1}{P} \right) = -NR(T_2 - T_1)$$

$$= -\frac{1000}{18} \times 8.314 \times 398.15 = -183.9 \text{ kJ}$$

(d) Ideal gas - constant volume

$$\frac{P_1 \underline{V}_1}{RT_1} = \frac{P_2 \underline{V}_2}{RT_2} \text{ here } \underline{V}_1 = \underline{V}_2; P_2 = 2P_1$$

$$\text{So again } \frac{P_1 \underline{V}_1}{T_1} = \frac{2P_1 \cdot \underline{V}_1}{T_2}; T_2 = 2T_1 = 796.3 \text{ K}.$$

$$Q = N \Delta \underline{U} = \frac{1000 \text{ g/kg}}{18 \text{ g/mol}} \times (34.4 - 8.314) \times (796.3 - 398.15) \times \frac{1}{1000}$$

$$C_V = C_P - R; Q = 577.0 \text{ kJ}$$

2.4

$$M_w \hat{U}_{w, f} - M_w \hat{U}_{w, i} = W_s = M_{\text{weight}} \times g \times 1 \text{ m}$$

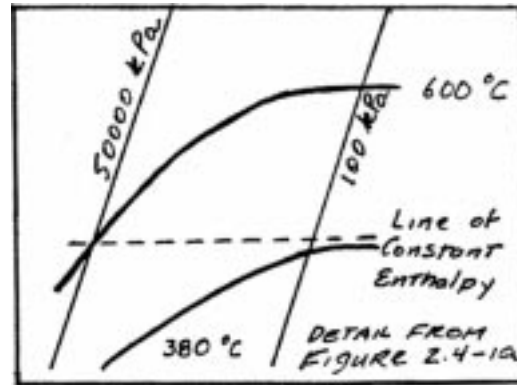
$$M_w = M_{\text{weight}} = 1 \text{ kg}$$

$$1 \text{ kg} \times C_p (T_f - T_i) = 1 \text{ kg} \times 9.807 \text{ m/s}^2 \times 1 \text{ m} \times \frac{1 \text{ J}}{\text{m}^2 \text{ kg/s}^2} = 9.807 \text{ J}$$

$$1 \text{ kg} \times 4.184 \text{ J/g K} \times \frac{1000 \text{ g}}{\text{kg}} \times \Delta T = 9.807$$

$$\Delta T = \frac{9.807}{4.184 \times 1000} \text{ K} = 2.344 \times 10^{-3} \text{ K}$$

- 2.5** From Illustration 2.3-3 we have that $\underline{H}(T_1, P_1) = \underline{H}(T_2, P_2)$ for a Joule-Thomson expansion. On the Mollier diagram for steam, Fig. 2.4-1a, the upstream and downstream conditions are connected by a horizontal line. Thus, graphically, we find that $T \sim 383 \text{ K}$. (Alternatively, one could also use the Steam Tables of Appendix III.)



For the ideal gas, enthalpy is a function of temperature only. Thus, $\underline{H}(T_1, P_1) = \underline{H}(T_2, P_2)$ becomes $\underline{H}(T_1) = \underline{H}(T_2)$, which implies that $T_1 = T_2 = 600^\circ\text{C}$.