

6. WAVE EQUATIONS AND WAVES

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MAXWELL'S EQUATIONS

An optical field propagating in a homogeneous, isotropic, linear medium, devoid of free charges and currents, must satisfy the following Maxwell's equations:

$$\nabla \times \mathbf{e} = -\frac{\mathbf{b}}{t} \quad (6.1)$$

$$\nabla \times \mathbf{b} = \frac{1}{c^2} \frac{\mathbf{e}}{t} \quad (6.2)$$

$$\nabla \cdot \mathbf{e} = 0 \quad (6.3)$$

$$\nabla \cdot \mathbf{b} = 0 \quad (6.4)$$

where the vectors \mathbf{e} and \mathbf{b} are the electric and magnetic field quantities, and c is the light velocity in the medium. In terms of the velocity c_v of light in vacuum

$$c = c_v/n, \quad (6.5)$$

where n is the refractive index of the (nonmagnetic) medium:

$$n = \sqrt{\epsilon_r}$$

and ϵ_r the relative dielectric constant

Taking the curl of (6.1) and substituting (6.2) into the result we find

$$\nabla \times \nabla \times \mathbf{e} = \nabla(\nabla \cdot \mathbf{e}) - \nabla^2 \mathbf{e} = -\frac{1}{c^2} \frac{\partial^2 \mathbf{e}}{\partial t^2} \quad (6.6)$$

With (6.3) we then find

$$\boxed{\nabla^2 \mathbf{e} = \frac{1}{c^2} \frac{\partial^2 \mathbf{e}}{\partial t^2}} \quad (6.7)$$

with an identical equation for the magnetic field:

$$\nabla^2 \mathbf{b} = \frac{1}{c^2} \frac{\partial^2 \mathbf{b}}{\partial t^2} \quad (6.8)$$

Eqs (6.6) and (6.7) are vector wave equations. Similar (scalar) equations must be obeyed by each component of \mathbf{e} and \mathbf{b} .

HELMHOLTZ EQUATION

If the field is monochromatic at frequency ω , \mathbf{e} and \mathbf{b} are represented by the phasors \mathbf{A} and \mathbf{B} :

$$\mathbf{e} = \text{Re} \{ \mathbf{A} \exp(-j \omega t) \}$$

$$\mathbf{b} = \text{Re} \{ \mathbf{B} \exp(-j \omega t) \}$$

Maxwell's equations for free space then become

$$\nabla \times \mathbf{E} = -j \omega \mathbf{B} \quad (6.9)$$

$$\nabla \times \mathbf{B} = \frac{-1}{c^2} j \omega \mathbf{E} \quad (6.10)$$

$$\nabla \cdot \mathbf{E} = 0 \quad (6.11)$$

$$\nabla \cdot \mathbf{B} = 0 \quad (6.12)$$

frequency ω .

Taking the curl ($\nabla \times$) of (6.1), using the relation

$$\nabla \times \nabla \times \mathbf{E} = \nabla (\nabla \cdot \mathbf{E}) - \nabla^2 \mathbf{E}$$

and substituting into (6.2) we find the well known *Helmholtz equation* :

$$\nabla^2 \mathbf{E} + k^2 \mathbf{E} = 0 \quad (6.13)$$

where the propagation constant k is given by

$$k = \omega / c = 2\pi / \lambda \quad (6.14)$$

and λ is the wave length in the medium.

SCALAR FIELDS

In this book we will mostly use scalar wave propagation as a model, with the field propagating nominally in the Z direction and E representing a single component in the XZ plane. Eq. (6.6) will then be written as the scalar equation :

$$\nabla^2 E + k^2 E = 0 \quad (6.15)$$

All the following equations in this section will be written as scalar equations.

COMPLEX ENVELOPE EQUATION

In this case e and b are defined as slowly time - varying phasors:

$$e = \text{Re} \{E(x,y,z,t)\exp(-j\omega t)\} \quad (6.16)$$

$$b = \text{Re}\{ B(x,y,z,t)\exp(-j \omega t) \} \quad (6.17)$$

where it is assumed that the time variation of $A(t)$ and $B(t)$ is slow compared to ω . Such slowly time-varying phasors are called complex envelopes in communication theory [Ref. 1] Substituting (6.16) into the scalar version of (6.7) we obtain:

$$\frac{\partial^2 E}{\partial z^2} = \frac{1}{c^2} \frac{\partial^2 E}{\partial t^2} - \frac{2j\omega}{c^2} \frac{\partial E}{\partial t} - k^2 E \quad (6.18)$$

$$\text{Assuming that } \left| \frac{\partial^2 E}{\partial t^2} \right| \ll \left| \frac{\partial E}{\partial t} \right| \quad (6.19)$$

we may write (6.18) as the *complex envelope equation* :

$$\boxed{\frac{\partial^2 E}{\partial z^2} + \frac{2j\omega}{c^2} \frac{\partial E}{\partial t} + k^2 E = 0} \quad (6.20)$$

COMPLEX PROFILE EQUATION

Often we assume that the field propagates nominally in the Z direction:

$$E(x,y,z,t) = E_e(x,y,z)\exp(jkz) \quad (6.21)$$

where the variation of the *complex profile* E_e with z is slow compared to k .

In that case

$$\frac{\partial^2 E}{\partial z^2} = \left\{ \frac{\partial^2 E_e}{\partial z^2} + 2jk \frac{\partial E_e}{\partial z} - k^2 E_e \right\} \exp(jkz) \quad (6.22)$$

may be written as

$$\frac{\partial^2 E}{\partial z^2} = (2jk \frac{\partial E_e}{\partial z} - k^2 E_e) \exp(jkz) \quad (6.23)$$

if we assume that

$$\left| \frac{2E}{z^2} \right| \ll k \left| \frac{E_e}{z} \right| \quad (6.24)$$

Substituting (6.23) into (6.15) we find the *complex profile equation*:

$$\frac{2E_e}{x^2} + \frac{2E_e}{y^2} + 2jk \frac{E_e}{z} = 0 \quad (6.25)$$

COMPLEX ENVELOPE/PROFILE EQUATION

Assuming that $E_e = E_e(x, y, z, t)$ is also slowly time varying, it is readily seen that we may "combine" (6.20) and (6.25) to obtain the *complex envelope/profile equation* :

$$\frac{2E_e}{x^2} + \frac{2E_e}{y^2} + 2jk \frac{E_e}{z} + \frac{2j}{c^2} \frac{E_e}{t} = 0 \quad (6.26)$$

which may also be written as

$$\frac{2E_e}{x^2} + \frac{2E_e}{y^2} + 2jk \frac{E_e}{z} + \frac{2jk}{c} \frac{E_e}{t} = 0 \quad (6.27)$$

PLANE WAVE

A scalar plane wave propagating in the direction of the wave vector \mathbf{k} is written as

$$E(x, y, z) = E_0 \exp(j\mathbf{k} \cdot \mathbf{r}) = E_0 \exp(jk_x x + jk_y y + jk_z z) \quad (6.28)$$

where \mathbf{r} is the position vector:

$$\mathbf{r} = x\mathbf{a}_x + y\mathbf{a}_y + z\mathbf{a}_z \quad (6.29)$$

and \mathbf{a}_x , \mathbf{a}_y , \mathbf{a}_z are unit vectors in the X and Y direction.

The variables k_x and k_y denote the lengths of the components of the wave vector k in the X and Y direction where

$$k = \omega/c = 2\pi/\lambda = \sqrt{k_x^2 + k_y^2 + k_z^2} \quad (6.30)$$

Eq. (6.30) follows directly by substituting (6.28) into (6.8). However, strictly speaking, (6.28) does not satisfy eq. (6.3) unless $k_x = k_y = 0$ (see [Ex. 6.1](#)). In scalar optics we assume that k_x and k_y are sufficiently small, so that (6.3) is satisfied. In other words, we assume that the wave propagates in a direction not too far off-axis. This is called paraxial propagation.

PARAXIAL APPROXIMATION

Fig. 6.1 shows the angles θ_x , θ_y , and θ_z are the angles that k makes with the X, Y and Z axis respectively. In terms of the direction cosines:

$$k_x = k \cos \theta_x, \quad k_y = k \cos \theta_y, \quad k_z = k \cos \theta_z \quad (6.31)$$

It is often more convenient to express this in terms of the azimuth angle ϕ (angle between k and its projection on the YZ plane) and the elevation angle θ (angle between k and its projection on the XZ plane), as illustrated in Fig. 6.1

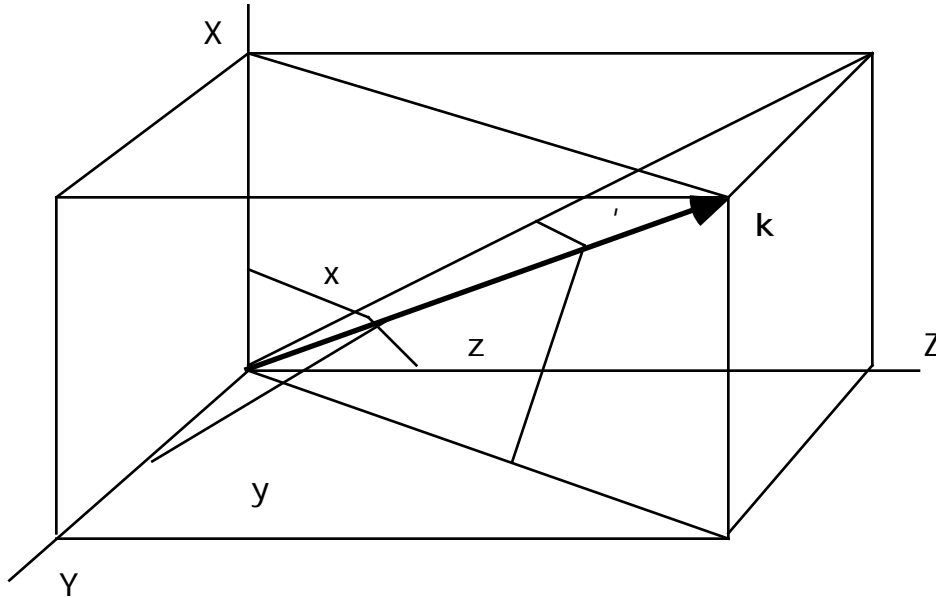


Fig. 6.1

$$k_x = k \sin \theta, \quad k_y = k \sin \theta', \quad k_z = k \sqrt{1 - \sin^2 \theta - \sin^2 \theta'} \quad (6.32)$$

In many cases k is directed at only a small angle with respect to the Z axis. This is called paraxial propagation and is characterized by $\theta, \theta' \ll 1$ i.e. k_x/k and k_y/k . In such cases we may write approximately:

$$k_z = \sqrt{k^2 - k_x^2 - k_y^2} \approx k - \frac{k_x^2}{2k} - \frac{k_y^2}{2k} \quad (6.33)$$

and

$$E(x, y, z) = E_0 \exp[(jk - \frac{k_x^2}{2k} - \frac{k_y^2}{2k})z] \exp(jk_x x + jk_y y) = E_0 \exp[jk(1 - \frac{\theta^2}{2} - \frac{\theta'^2}{2})z] \exp(jk_x x + jk_y y) \quad (6.34)$$

EVANESCENT WAVE

Note from (6.30) that, if $k_x^2 + k_y^2 > k^2$, the z-component of k i.e. k_z becomes imaginary. The wave then propagates in the +Z direction as $\exp(kz)$ or $\exp(-kz)$:

$$E(x,y,z) = E_0 \exp(\pm k_z z) \exp(jk_x x + jk_y y) \quad (6.35)$$

The "plus z" version is obviously physically impossible for all $z > 0$, because of the implied unlimited growth of the wave. The "minus z" version is possible, provided the wave originates from a current or charge carrying surface, located at a finite value of z . This kind of wave is called an evanescent wave and decays quickly away from the surface that originated it.

WAVE FRONTS

A surface on which the phase of the wave is constant is called a wavefront. For the plane wave of (6.28), the wavefronts are obviously given by the surfaces

$$\frac{\mathbf{k}}{k} \cdot \mathbf{r} = d \quad (6.36)$$

where d is a real constant. As shown in Fig. 6.2, these surfaces are planes perpendicular to \mathbf{k} , a distance d from the origin.

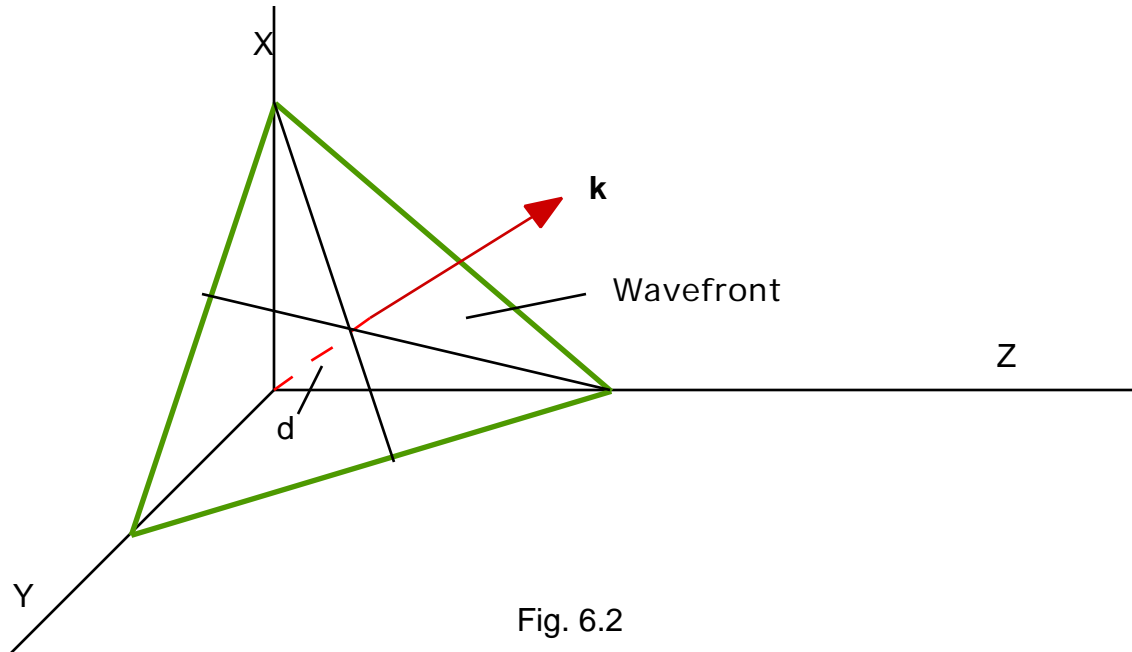


Fig. 6.2

SPHERICAL WAVE

In the case of spherical waves the field is given by

$$E(x,y,z) = \frac{1}{r} \exp(\pm jkr) = \frac{1}{r} \exp(\pm jk\sqrt{x^2+y^2+z^2}) \quad (6.37)$$

where the plus sign denotes a diverging wave (going out from the source at $z=0$), the minus sign a converging wave (coming in to the sink at $z=0$). As shown in [Ex 6.2](#), expression 6.37 satisfies the Helmholtz equation.

It is readily seen from (6.37) that the wavefronts of a spherical wave are spheres:

$$r = \text{constant} \quad (6.38)$$

In paraxial propagation the field does not propagate at too steep an angle i.e., it is limited to a region where $x^2 \ll z^2$, $y^2 \ll z^2$, and we may write:

$$E(x,y,z) = \frac{1}{z} \exp(\pm jkz) \exp(\pm jkx^2/2z \pm jky^2/2z)$$

(6.39)

As before, the plus sign denotes a diverging wave, the minus sign a converging wave. The factor $\exp(\pm jkz)$, being independent of x and y , is frequently left out. The amplitude factor $1/r$ is approximated by $1/z$ while the phase factor (being more sensitive to small changes in r) is approximated to order x^2 and y^2 . Note that, in the factor $\exp(\pm jkx^2/2z \pm jky^2/2z)$, z is the radius of the wavefront through the point z . The factor itself is an approximation for the phase in the plane perpendicular to the Z axis at z . In general, factors such as

$$\exp(\pm jkx^2/2R \pm jky^2/2R)$$

denote a spherical wavefront of radius R whereas

$$\exp(\pm jkx^2/2R_1 \pm jky^2/2R_2)$$

denotes a wavefront with radius R_1 in the X direction and radius R_2 in the Y direction. A heuristic explanation of (6.39) - limited to the XZ plane - is shown in Fig. 6.3

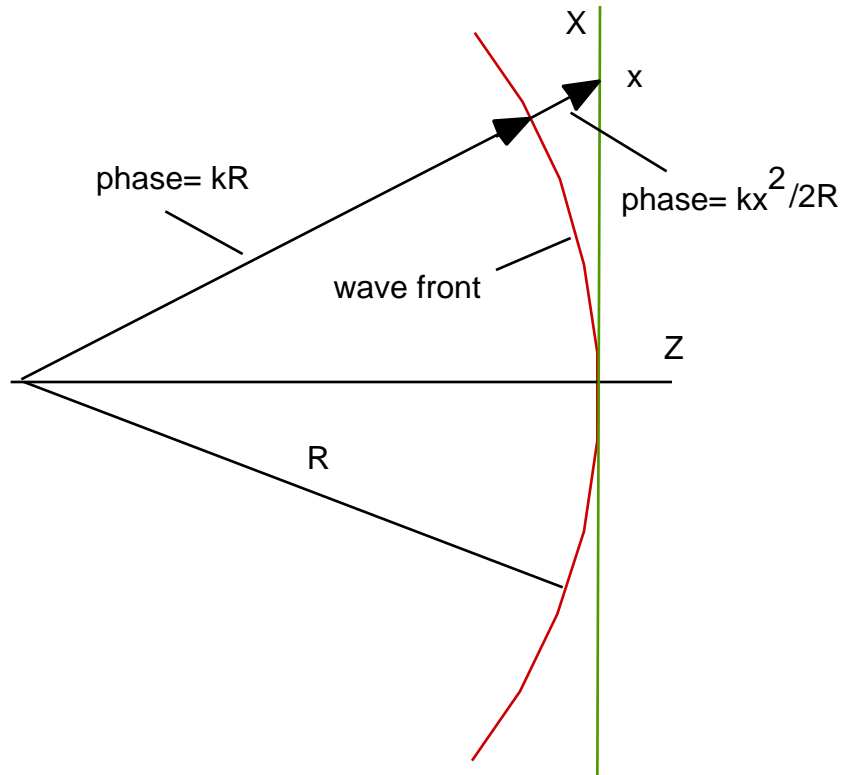


Fig. 6.3

CYLINDRICAL WAVE

A cylindrical wave is essentially a one-dimensional spherical wave, i.e., it is independent of y and varies in the XZ plane only, with $r = \sqrt{x^2+z^2}$. The amplitude is then proportional to $1/\sqrt{r}$ rather than $1/r$, i.e.

$$E(x,y,z) = \frac{1}{\sqrt{r}} \exp(\pm jkr) = \frac{1}{\sqrt{r}} \exp(\pm jk\sqrt{x^2+z^2}) \quad (6.40)$$

As shown in [Ex. 6.3](#), eq.(6.40) satisfies the Helmholtz equation for $kr \gg 1$, i.e., $r \gg \lambda$.

It follows immediately from (6.40) that the wavefronts of a cylindrical wave are cylinders with axes along y :

$$r = \sqrt{x^2+z^2} = \text{constant}. \quad (6.41)$$

In the paraxial approximation (6.40) becomes:

$$E(x,y,z) = \frac{1}{\sqrt{z}} \exp(\pm jkz) \exp(\pm jkx^2/2z) \quad (6.42)$$

CIRCULAR GAUSSIAN BEAM

The field of a circular Gaussian beam at z is given by :

$$E(x,y,z) = E_0 \frac{w_0}{w_z} \exp[+jkz - j(z) + j \frac{kr^2}{2R_z} + \frac{r^2}{w_z^2}] \quad (6.43)$$

where w_0 is the waist (beam radius where the amplitude has decreased to $1/e$ of the maximum value) at $z=0$; $w_z = w_z(z)$, the waist at z , and r is a transverse coordinate $r = \sqrt{x^2+y^2}$. The function (z) is a slowly varying phase term. The parameter $R_z = R_z(z)$ is called the radius of curvature of the wavefront at z , in analogy to the paraxial approximation (6.37) of the spherical wave (6.39). However, unlike (6.37), the radius of curvature is not equal to the distance z from the origin: the wavefronts are spheres, but they are not concentric. It is shown in [Ex. 6.4](#) that, in order for (6.43) to satisfy the complex profile equation (6.25), the following relations must hold:

$$w_z = w_0 \sqrt{1 + \frac{z^2}{z_0^2}} \quad (6.44)$$

$$R_z = z \left(1 + \frac{z_0^2}{z^2} \right) \quad (6.45)$$

$$(z) = \tan^{-1} \frac{z}{z_0} \quad (6.46)$$

where

$$z_0 = k \frac{w_0^2}{2} \quad (6.47)$$

Fig. 6.3 illustrated the XZ crosssection of a propagating circular Gaussian beam. The $1/e$ contour line is stylized. The "break point" z_0 indicates where the beam has spread to $\sqrt{2}$ its initial width.

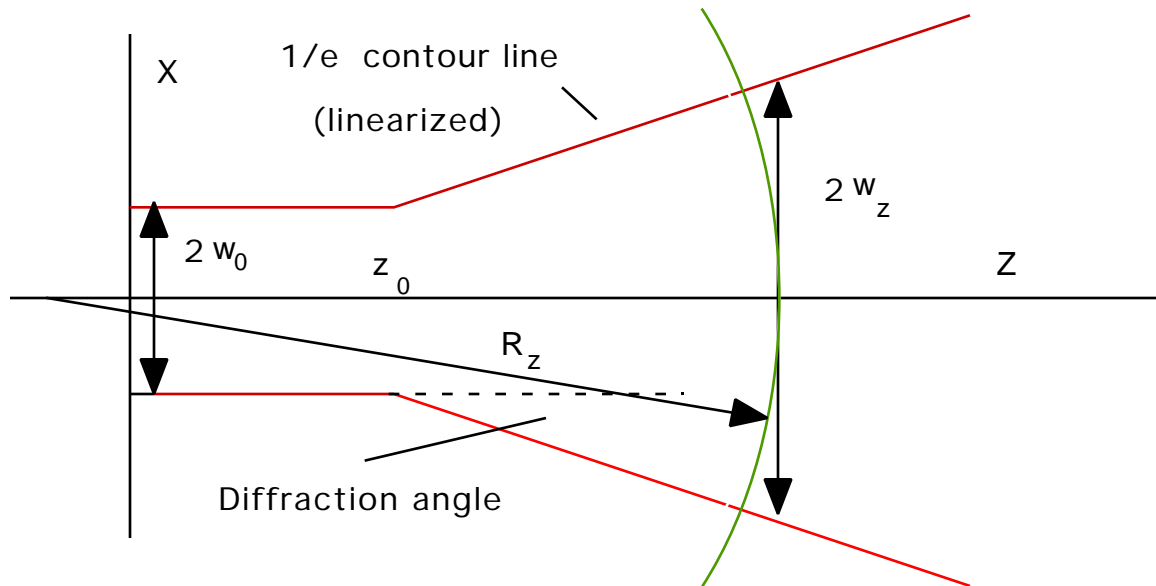


Fig. 6.4

ELLIPTICAL GAUSSIAN BEAM

The field of an elliptical Gaussian beam is given by:

$$E(x,y,z) = E_0 \sqrt{\frac{w_{0x}w_{0y}}{w_{zx}w_{zy}}} \exp(+jkz) \times$$

$$\exp[-j \frac{x^2}{2R_{zx}} + j \frac{kx^2}{2R_{zx}} + \frac{x^2}{w_{zx}^2}] \exp[-j \frac{y^2}{2R_{zy}} + j \frac{ky^2}{2R_{zy}} + \frac{y^2}{w_{zy}^2}] \quad (6.48)$$

where w_{0x} and w_{0y} are the waists at the origin in the XZ plane and YZ plane respectively; w_{zx} and w_{zy} are those waists at z ; and R_{zx} and R_{zy} are the radii of curvature in the XZ plane and YZ plane at z .

The following relations apply:

$$w_{zxy} = w_{oxy} \sqrt{1 + \frac{z_{xy}^2}{z_0^2}} \quad (6.49)$$

$$R_{zxy} = z \left(1 + \frac{z_{oxy}^2}{z^2}\right) \quad (6.50)$$

$$\phi(z) = \frac{1}{2} \tan^{-1} \left(\frac{z}{z_{oxy}}\right) \quad (6.51)$$

where

$$z_{oxy} = k \frac{w_{oxy}^2}{2} \quad (6.52)$$

and the subscript xy applies to either x or y.

EXAMPLES

EX 6.1

We will first show that, strictly speaking, a plane wave traveling in an direction other than Z, while polarized in the X direction, does not satisfy the Helmholtz equation.

The electric field vector is given by

$$\mathbf{E}(x,y,z) = E_0 \mathbf{a}_x \exp(-jk \cdot \mathbf{r}) = E_0 \mathbf{a}_x \exp(-jk_x x - jk_y y - jk_z z)$$

Hence:

$$\nabla^2 \mathbf{E} = \frac{\partial^2 \mathbf{E}}{\partial x^2} + \frac{\partial^2 \mathbf{E}}{\partial y^2} + \frac{\partial^2 \mathbf{E}}{\partial z^2} = -jk_x^2 E_0 \exp(-jk_x x - jk_y y - jk_z z) \mathbf{a}_x - jk_y^2 E_0 \exp(-jk_x x - jk_y y - jk_z z) \mathbf{a}_y - jk_z^2 E_0 \exp(-jk_x x - jk_y y - jk_z z) \mathbf{a}_z \neq 0$$

which completes the proof.

A more general statement is that for $\nabla^2 \mathbf{E} = 0$ to be zero, \mathbf{E} must be perpendicular to the direction of propagation \mathbf{k} . This may be shown as follows. Let

$$\mathbf{E}(x,y,z) = E_0 \exp(-jk \cdot \mathbf{r}) =$$

$$(E_{0x} \mathbf{a}_x + E_{0y} \mathbf{a}_y + E_{0z} \mathbf{a}_z) \exp(-jk_x x - jk_y y - jk_z z)$$

Hence

$$\nabla \cdot \mathbf{E} = \frac{E_x}{x} + \frac{E_y}{y} + \frac{E_z}{z} = -j(k_x E_{0x} + k_y E_{0y} + k_z E_{0z}) \exp(-jk \cdot \mathbf{r})$$

This can only equal zero if $(k_x E_{0x} + k_y E_{0y} + k_z E_{0z}) = 0$ and hence \mathbf{k} must be perpendicular to \mathbf{E}_0

Ex 6.2

The spherical wave $E(x,y,z) = \frac{1}{r} \exp(\pm jkr)$ satisfies the Helmholtz equation $\nabla^2 E + k^2 E = 0$.

It is more convenient to recast the Helmholtz equation in spherical coordinates. Because $E(x,y,z)$ only depends on r , we use the following expression for the Laplacian [\[Ref 2\]](#)

$$\nabla^2 E = \frac{1}{r^2} \frac{d}{dr} \left(r^2 \frac{dE}{dr} \right) \quad (6.2.1)$$

After some algebra, we find that

$$\frac{1}{r^2} \frac{d}{dr} \left(r^2 \frac{dE}{dr} \right) = -k^2 E$$

so that the Helmholtz equation is satisfied.

Ex. 6.3

We will show that the cylindrical wave of 6.21 satisfies the Helmholtz equation $\nabla^2 E + k^2 E = 0$ if $kr \gg 1$

We use a cylindrical coordinate system with the axes along Y . Taking into account that E only depends on $r = \sqrt{x^2 + z^2}$, the Helmholtz equation may be written as

$$\frac{1}{2kr} \frac{1}{r} \frac{E}{r} + k^2 E = 0 \quad (6.3.1)$$

Substituting

$$E(x,y,z) = \frac{1}{\sqrt{r}} \exp(\pm jkr)$$

into (6.3.2), we find

$$-k^2 E \left[1 - \frac{1}{4k^2 r^2} \right] + k^2 E = 0 \quad (6.3.2)$$

We see that (6.3.2) is satisfied if $kr \gg 1$.

Ex. 6.4

Propagation of a circular Gaussian beam.

We assume that the beam is given by

$$E(x,y,z) = A(z) \exp[-a(z)(x^2+y^2)] \exp(jkz) \quad (6.4.1)$$

so that the complex profile E_e is

$$E_e = A(z) \exp[-a(z)(x^2+y^2)] \quad (6.4.2)$$

Applying the complex profile equation

$$\frac{\partial^2 E_e}{\partial x^2} + \frac{\partial^2 E_e}{\partial y^2} + 2jk \frac{\partial E_e}{\partial z} = 0 \quad (6.4.3)$$

to (6.4.2) we find:

$$-4a + 4a^2 x^2 + 4a^2 y^2 + 2jk \frac{1}{A} \frac{dA}{dz} - 2jk x^2 \frac{da}{dz} - 2jk y^2 \frac{da}{dz} = 0 \quad (6.4.4)$$

Setting the constant terms and the coefficients of x^2 , y^2 separately equal to zero, we obtain:

$$-2a + jk \frac{1}{A} \frac{dA}{dz} = 0 \quad (6.4.5)$$

$$2a^2 - jk \frac{da}{dz} = 0 \quad (6.4.6)$$

From (6.4.6) it follows immediately that

$$a(z) = \frac{1}{w_0^2 + 2jz/k} \quad (6.4.7)$$

where $w_0^2 = a(z=0)$, the beam radius at the origin.

Eq (6.4.7) may be written as:

$$a(z) = \frac{1}{w_0^2 \left(1 + \frac{4z^2}{k^2 w_0^4}\right)} - \frac{jk}{2z \left(1 + \frac{k^2 w_0^4}{4z^2}\right)} \quad (6.4.8)$$

Defining

$$z_0 = kw_0^2/2 = w_0^2/ \quad (6.4.9)$$

we may write

$$a(z) = \frac{1}{w^2(z)} - \frac{jk}{2R(z)} \quad (6.4.10)$$

where

$$w^2(z) = w_0^2 \left(1 + \frac{z^2}{z_0^2}\right) \quad (6.4.11)$$

$$R(z) = z \left(1 + \frac{z_0^2}{z^2}\right) \quad (6.4.12)$$

Combining (6.4.5) and (6.4.6) gives

$$\frac{1}{A} \frac{dA}{dz} = \frac{1}{a} \frac{da}{dz} \quad (6.4.12)$$

whence $A = Ca$

$$\text{At } z=0, A=A_0 \text{ and } a = \frac{1}{w_0^2} \text{ hence } C = A_0 w_0^2$$

With (6.4.7) it then follows that

$$A(z) = \frac{A_0 w_0^2}{w_0^2 + 2jz/k} = \frac{A_0 w_0^2}{\sqrt{w_0^4 + 4z^2/k^2}} \exp[-j \tan^{-1} \left(\frac{2z}{kw_0^2} \right)]$$

(6.4.13)

With (6.4.9) and (6.4.11) this may be written as

$$A(z) = A_0 \frac{w_0}{w(z)} \exp(-j(z)) \quad (6.4.14)$$

where

$$(z) = \tan^{-1} \left(\frac{z}{z_0} \right) \quad (6.4.15)$$

REFERENCES

1. S. Haykin, *Communication Systems*, 3rd ed., Wiley, New York, 1994
2. D. K. Cheng, *Field and Wave Electromagnetics*, 2nd ed., Addison-Wesley, New York, 1989.

