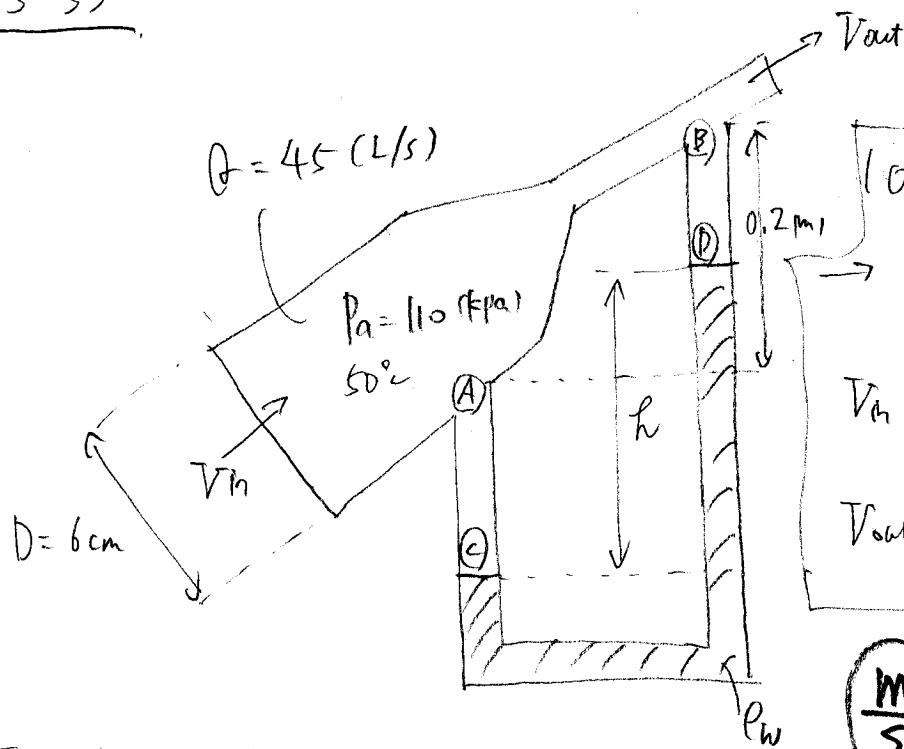


5-55



Velocity at Inlet & Exit.

$$10000 \text{ (L/s)} = 10 \text{ (m}^3\text{/s)}$$

$$45 \text{ (L/s)} = 4.5 \times 10^{-3} \text{ (m}^3\text{/s)}$$

$$V_{in} = \frac{Q}{A_{in}} = \frac{4.5 \times 10^{-3}}{\left(\frac{0.06}{2}\right)^2 \pi} = 15.9 \text{ m/s}$$

$$V_{out} = \frac{Q}{A_{out}} = \frac{4.5 \times 10^{-3}}{\left(\frac{0.04}{2}\right)^2 \pi} = 35.9 \text{ m/s}$$

$$\left(\frac{\text{m}}{\text{s}}\right) = \frac{\text{m}^3}{\text{s} \cdot \text{m}^2}$$

Use Bernoulli eqn.

$$A-B: \frac{1}{2} \rho_a V_{in}^2 + P_A + \rho_a g z_A = \frac{1}{2} \rho_a V_{out}^2 + P_B + \rho_a g z_B \quad \text{--- (1)}$$

$$C-D: P_A + \rho_w g z_C = P_B + \rho_w g z_D \quad \text{--- (2)}$$

From (2)

$$P_A - P_B = \rho_w g (z_D - z_C) = \rho_w g h \quad \text{--- (3)}$$

From (1)

$$P_A - P_B = \rho_a g (z_B - z_A) + \frac{1}{2} \rho_a (V_{out}^2 - V_{in}^2) \quad \text{--- (4)}$$

Equate (3) and (4)

$$\rho_w g h = \frac{1}{2} \rho_a (V_{out}^2 - V_{in}^2) + \rho_a g (z_B - z_A)$$

$$\rightarrow h = \frac{\rho_a}{\rho_w g} \left\{ \frac{1}{2} (V_{out}^2 - V_{in}^2) + g (z_B - z_A) \right\} \quad \text{--- (5)}$$

We need to get  $\rho_a$  since we are given the pressure.

$$\rightarrow P_a = \rho_a R T \rightarrow \rho_a = \frac{P_a}{R T} = \frac{110 \times 10^3}{0.287 \times (50 + 273)} = 1.106$$

$$z_B - z_A = 0.2 \text{ m}$$

$$\rho_a = 1000 \text{ (kg/m}^3\text{)}$$

are known.

→ Plug these value into (5)

$$h = 0.0627 \text{ (m)} //$$

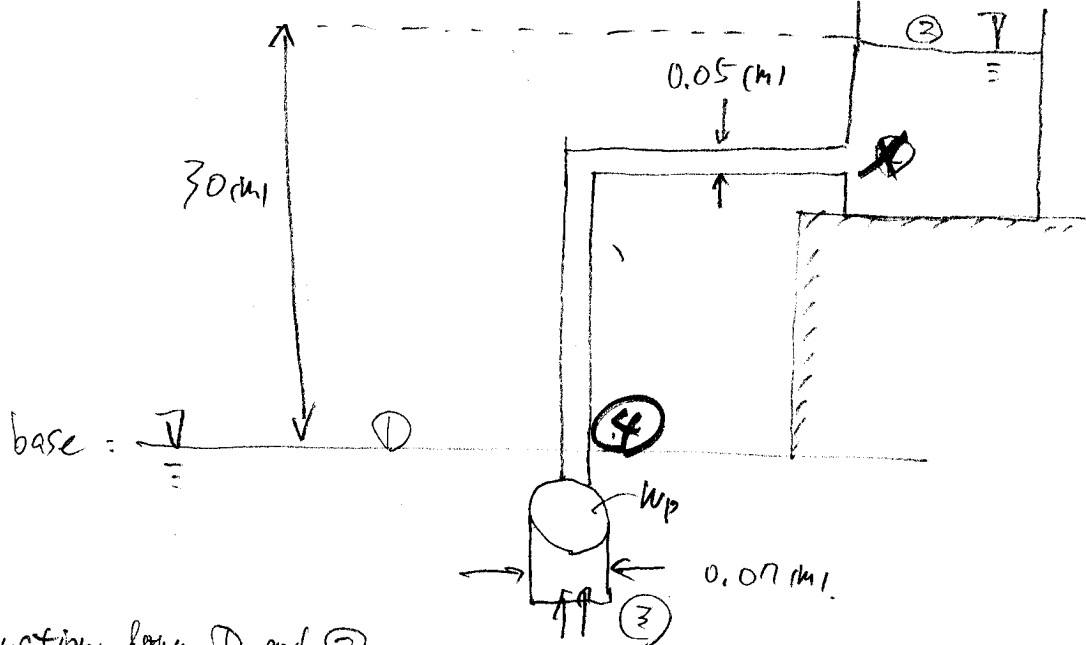
Use (3) to get

$$P_A - P_B = \rho_w g h$$

$$= 614 \text{ (Pa)} //$$

5-69

$$\begin{aligned}
 W_p &= 3 \text{ (kW)} \\
 &= 3000 \text{ (W)} \\
 &= 3000 \left( \frac{\text{J}}{\text{s}} \right) \\
 &= 3000 \left( \frac{\text{N} \cdot \text{m}}{\text{s}} \right) \\
 &= 3000 \left( \frac{\text{kg} \cdot \text{m}^2}{\text{s}^3} \right)
 \end{aligned}$$



(a) State from energy equation between 1 and 2

$$\dot{m} \left( \frac{P_1}{\rho} + \alpha \frac{V_1^2}{2} + g z_1 \right) + W_{\text{pump}} = \dot{m} \left( \frac{P_2}{\rho} + \alpha \frac{V_2^2}{2} + g z_2 \right) + W_{\text{turb}} + \dot{E}_{\text{mech. loss}}$$

D. 2 : Open to atmosphere  $\rightarrow P_1, P_2 = 0$

$W_{\text{turb}} = 0$   $\because$  no turbine

$$\rightarrow \left[ \alpha \frac{\dot{m} V_1^2}{\rho^2} + W_{\text{pump}} = \alpha \frac{\dot{m} V_2^2}{\rho^2} + \dot{m} g z_2 + \dot{E}_{\text{mech. loss}} \right]$$

$V_1, V_2 = 0$  : Free-surface is large enough.

$$\therefore W_{\text{pump, u}} = W_{\text{pump}} - \dot{E}_{\text{mech. loss}} = \dot{m} g z_2$$

Given that  $W_{\text{pump, u}} = 3000 \times 0.7 = 2100 \left[ \frac{\text{kg} \cdot \text{m}^2}{\text{s}^3} \right]$

$$\therefore \dot{m} = \frac{W_{\text{pump, u}}}{g z_2} = \frac{2100}{9.8 \times 30} = 7.142 \text{ [kg/s]}$$

$$\therefore \dot{Q} = \frac{1}{\rho} \cdot \dot{m} = \frac{1}{1000} \times 7.142 = 7.142 \times 10^{-3} \text{ m}^3/\text{s}$$

(b) Energy eqn between 3 and 4

$$\underbrace{\dot{m} \left( \frac{P_3}{\rho} + \alpha \frac{V_3^2}{2} + g z_3 \right) + W_{\text{pump}}}_{\text{Inlet}} = \underbrace{\dot{m} \left( \frac{P_4}{\rho} + \alpha \frac{V_4^2}{2} + g z_4 \right) + W_{\text{turb}} + \dot{E}_{\text{mech. loss}}}_{\text{Exit}} \quad \text{--- } \star$$

$$A_3 \textcircled{3} : (0.035)^2 \pi \times V_3 = 7.142 \times 10^{-7} \rightarrow V_3 = 1.856$$

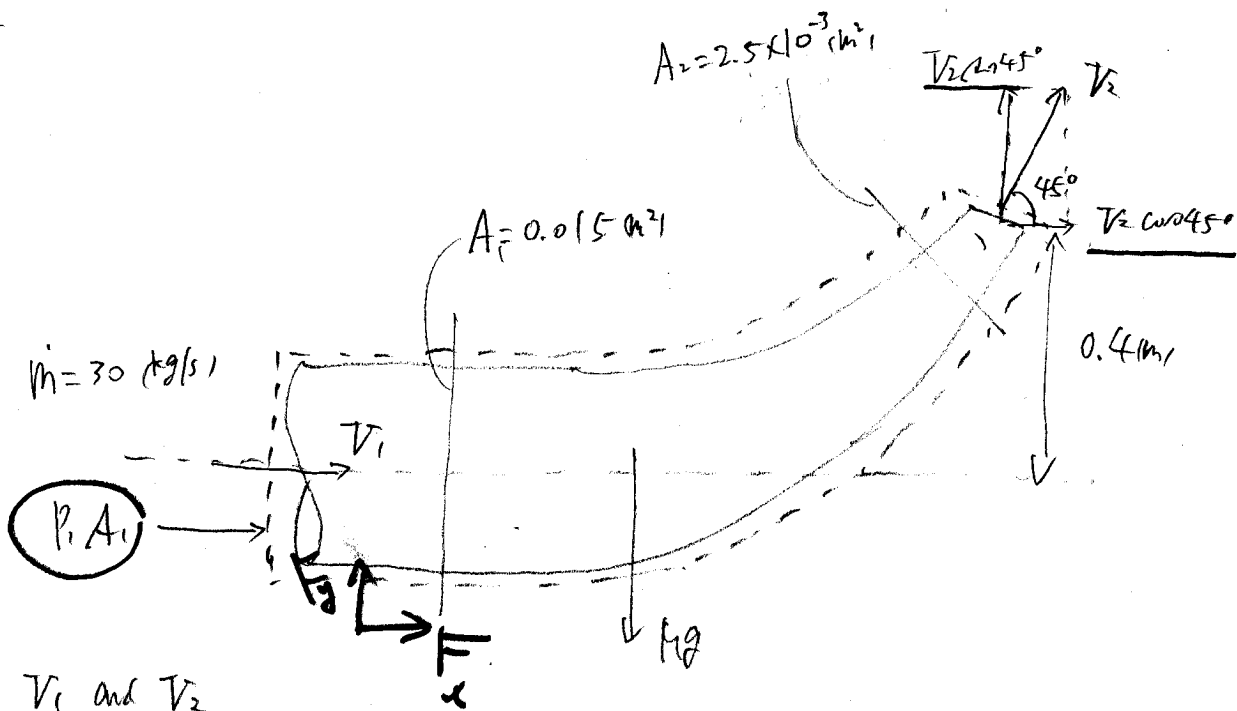
$$A_4 \textcircled{4} : (0.025)^2 \pi \times V_4 = 7.142 \times 10^{-7} \rightarrow V_4 = 3.637$$

Also,  $W_{\text{pump}} - E_{\text{mech. loss}} = \underline{2100}$  (from (a))

Plug those values into  $\textcircled{4}$

$$\underline{P_3 - P_4 = 289.21 \text{ (kPa)}} //$$

6-25



Obtain  $V_1$  and  $V_2$

$$\dot{m} \left[ \frac{\text{kg}}{\text{s}} \right] = \rho \left[ \frac{\text{kg}}{\text{m}^3} \right] \times Q \left[ \frac{\text{m}^3}{\text{s}} \right] \rightarrow Q = \frac{\dot{m}}{\rho} = \frac{30}{1000} = 0.03 \left[ \frac{\text{m}^3}{\text{s}} \right]$$

$$\rightarrow \left\{ \begin{array}{l} Q = A_1 V_1 \rightarrow V_1 = \frac{Q}{A_1} = \frac{0.03}{0.015} = 2 \text{ m/s} \\ Q = A_2 V_2 \rightarrow V_2 = \frac{Q}{A_2} = \frac{0.03}{2.5 \times 10^{-3}} = 12 \text{ m/s} \end{array} \right.$$

Use Bernoulli equation to get pressure at inlet.

$$\underbrace{P_1 + \frac{1}{2} \rho V_1^2 + \rho g z_1}_{\text{inlet}} = \underbrace{P_2 + \frac{1}{2} \rho V_2^2 + \rho g z_2}_{\text{exit}}$$

$$\rightarrow P_1 = \frac{1}{2} \rho (V_2^2 - V_1^2) + \rho g (z_2 - z_1) = 73920 \text{ [Pa]}$$

State down steady state linear momentum eqn.

$$\sum \vec{F} = \sum_{\text{out}} \beta \dot{m} \vec{V} - \sum_{\text{in}} \beta \dot{m} \vec{V}$$

$\rightarrow$  Decompose it into horizontal and vertical components

$$\text{horizontal} : F_x + P_1 A_1 = \beta \dot{m} V_2 \cos 45^\circ - \beta \dot{m} V_1$$

$$\text{vertical} : F_y - Mg = \beta \dot{m} V_2 \sin 45^\circ$$

with  $\beta = 1.03$

$$\rightarrow F = \sqrt{F_x^2 + F_y^2} = \underline{1.18 \text{ (kN)}}$$

# Dimensional Analysis

$F_r$  must be the same between model and prototype.

$$\rightarrow F_r |_{\text{model}} = F_r |_{\text{prototype}}$$

$$\rightarrow \frac{V_m}{\sqrt{g L_m}} = \frac{V_p}{\sqrt{g L_p}} \rightarrow V_p = \frac{\sqrt{g L_p}}{\sqrt{g L_m}} V_m = \sqrt{\frac{L_p}{L_m}} V_m$$

Given that  $L_p = 25 L_m$   $\rightarrow V_p = \sqrt{\frac{25 L_m}{L_m}} V_m = 5 \times 5 = 25 \text{ (ft/s)}$

$C_D$  (Drag coefficient) must be the same between model and prototype.

$$\rightarrow C_D |_{\text{model}} = C_D |_{\text{prototype}}$$

$$\rightarrow \frac{F_m}{\frac{1}{2} \rho_m V_m^2 A_m} = \frac{F_p}{\frac{1}{2} \rho_p V_p^2 A_p}$$

$\rightarrow$  Assume  $\rho_m \approx \rho_p$  then

$$\frac{F_p}{F_m} = \frac{V_p^2 A_p}{V_m^2 A_m}$$

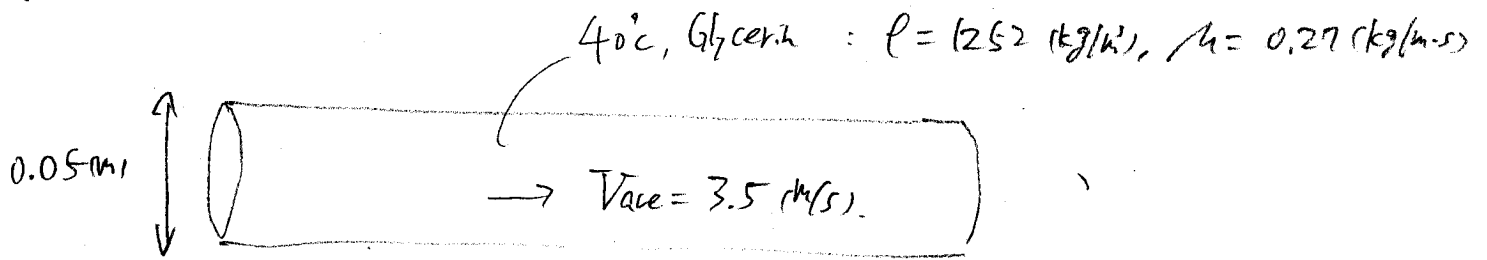
Replace  $A_p = L_p^2$ ,  $A_m = L_m^2$ , then

$$\frac{F_p}{F_m} = \left(\frac{V_p}{V_m}\right)^2 \left(\frac{L_p}{L_m}\right)^2$$

$$= 25 \times (25)^2 = (25)^3$$

$$\rightarrow F_p = (25)^3 F_m$$

f-46



Check the Re first to determine if the flow is laminar or turbulent.

$$Re = \frac{\rho V D}{\mu} = \frac{1252 \times 3.5 \times 0.05}{0.27} = 811.48 : \text{laminar (} \because Re < 2300 \text{)}$$

$$\begin{aligned} \Delta p &= \frac{32 \mu L V_{ave}}{D^2} = \frac{32 \times 0.27 \times 10 \times 3.5}{(0.05)^2} = 120960 \text{ Pa} \\ &= \underline{120.96 \text{ (kPa)}} \end{aligned}$$

Or

$$f = \frac{64}{Re} = \frac{64}{811.48}$$

then

$$\Delta P_L = f \frac{L}{D} \frac{\rho V_{ave}^2}{2}$$

Yields the same result!!