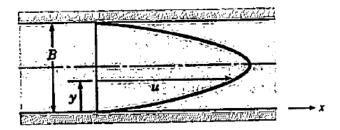
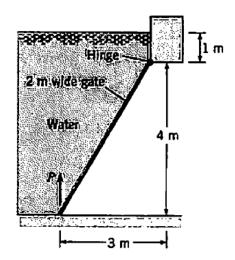
1. Shear stress

Given $u = 10y^{1/6}$, where u is the velocity of water (20°C) in meters per second and y is the distance from the boundary in mm, determine the shear stress in the water at y = 2 mm.



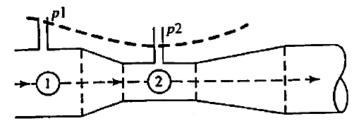
2. Hydrostatic pressure on a plane surface Determine *P* to just start opening the 2-m wide gate.



3. Bernoulli equation

A constriction in a pipe will cause the velocity to rise and the pressure to fall at section 2 in the throat. The pressure difference is a measure of the flow rate through the pipe. The smoothly necked-down system shown in Fig. E3.23 is called a *venturi tube*. Find an expression for the mass flux in the tube as a function of the pressure change.

E3.23



4. Fluid kinematics

An idealized velocity field is given by the formula

$$V = 4txi - 2t^2yj + 4xzk$$

Is this flow field steady or unsteady? Is it two- or three-dimensional? At the point (x, y, z) = (-1, 1, 0), compute the acceleration vector

Answer

1. Shear stress

Information and assumptions

$$\mu=10^{-3}\;\mathrm{N}\!\cdot\!\mathrm{s/m^2}$$

Find

shear stress at y = 2 mmStress-strain relationship

$$\begin{array}{rcl} \tau &=& \mu du/dy \\ du/dy &=& (1/6)(10)(y)^{-5/6} \; {\rm s}^{-1} \\ &=& (1/6)(10)(.002)^{-5/6} \; {\rm s}^{-1} \\ &=& (10/6)(177.5) \; {\rm s}^{-1} \\ \tau &=& (10^{-3} \; {\rm N} \cdot {\rm s/m^2})(10/6)(177.5) \; {\rm s}^{-1} = \underline{0.296 \; {\rm N/m^2}} \end{array}$$

2. Hydrostatic pressure on a plane surface Information and assumptions

provided in problem statement

Find

force P required to begin to open gate

Solution

The length of gate is $\sqrt{4^2 + 3^2} = 5 \text{ m}$

$$\bar{y} = 2.5 \text{ m} + 5/4 \text{ m}$$

 $= 3.75 \text{ m}$
 $F = \bar{p}A$
 $= (4/5)(3.75)(9,810)(2 \times 5)$
 $= 294,300 \text{ N}$
 $= 294.3 \text{ kN}$
 $y_{cp} - \bar{y} = I/(\bar{y}A)$
 $= 2 \times (5^3/12)/(3.75 \times 2 \times 5)$
 $= 0.555 \text{ m}$

Sum moments about hinge:

$$\sum M_{\text{hinge}} = 0$$

$$F \times (2.5 + .555) + 3P = 0$$

$$294.3(3.055) + 3P = 0$$

$$\underline{P = 300 \text{ kN}}$$

3. Bernoulli equation

If the tube is horizontal, $z_1 = z_2$ and we can solve for V_2 :

$$V_2^2 - V_1^2 = \frac{2\Delta p}{\rho} \qquad \Delta p = p_1 - p_2 \tag{1}$$

We relate the velocities from the incompressible continuity relation:

$$A_1V_1=A_2V_2$$

ог

$$V_1 = \beta^2 V_2$$
 $\beta = \frac{D_2}{D_1}$ (2)

Combining (1) and (2), we obtain a formula for the velocity in the throat:

$$V_2 = \left[\frac{2 \, \Delta p}{\rho (1 - \beta^4)} \right]^{1/2} \tag{3}$$

The mass flux is given by

$$\dot{m} = \rho A_2 V_2 = A_2 \left(\frac{2\rho \, \Delta p}{1 - \beta^4} \right)^{1/2}$$
 (4)

4. Fluid kinematics

- (a) The flow is <u>unsteady</u> because time t appears explicitly in the components.
- (b) The flow is three-dimensional because all three velocity components are nonzero.
- (c) Evaluate, by laborious differentiation, the acceleration vector at (x, y, z) = (-1, +1, 0).

$$\frac{du}{dt} = \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = 4x + 4tx(4t) - 2t^2y(0) + 4xz(0) = 4x + 16t^2x$$

$$\frac{dv}{dt} = \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = -4ty + 4tx(0) - 2t^2y(-2t^2) + 4xz(0) = -4ty + 4t^4y$$

$$\frac{dw}{dt} = \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = 0 + 4tx(4z) - 2t^2y(0) + 4xz(4x) = 16txz + 16x^2z$$
or:
$$\frac{dV}{dt} = (4x + 16t^2x)\mathbf{i} + (-4ty + 4t^4y)\mathbf{j} + (16txz + 16x^2z)\mathbf{k}$$
at $(x, y, z) = (-1, +1, 0)$, we obtain
$$\frac{dV}{dt} = -4(1 + 4t^2)\mathbf{i} - 4t(1 - t^3)\mathbf{j} + 0\mathbf{k} \quad Ans. (c)$$