## November 4, 2013



Fluids-ID

Quiz 10. An oil film drains steadily down the side of a vertical wall, as shown on the Figure. After an initial development at the top of the wall, the film becomes independent of z and of constant thickness ( $\delta$ ). Assume that  $w =$  $w(x)$ , pressure gradient is negligible, and shear stress ( $\tau$ ) at the free surface is zero.

- A. Solve Navier-Stokes for  $w(x)$ .
- B. If the oil is SAE 30W ( $\rho$  = 891 kg/m<sup>3</sup> and  $\mu$  = 0.29 kg/m⋅s),  $\delta$  = 2 mm, and the plate width (into the paper)  $W=1$  m and height  $H=2$  m, find (a) the maximum velocity  $w_{max}$ , (b) flow rate Q, (c) average velocity  $\bar{w}$ , (d) shear stress on the wall  $\tau_w$ , and (e) the friction drag force acting on the plate  $D$ .





Note: Attendance (+2 points), format (+1 point) Part A:

The assumption of parallel flow,  $u = v = 0$  and  $w = w(x)$ , satisfies continuity and makes the x and z momentum equations irrelevant. We are left with the z momentum equation

$$
\rho\left(0+0\times\frac{\partial w}{\partial x}+0\times\frac{\partial w}{\partial y}+w\times 0\right)=-(0)-\rho g+\mu\left(\frac{\partial^2 w}{\partial x^2}+0+0\right)
$$

There no convective acceleration and the pressure gradient is negligible due to the free surface. We are left with a second order linear differential equation for  $w(x)$ 

$$
\frac{d^2w}{dx^2} = \frac{\rho g}{\mu}
$$

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Integrating

$$
\frac{dw}{dx} = \frac{\rho g}{\mu} x + C_1
$$
  

$$
w = \frac{\rho g}{2\mu} x^2 + C_1 x + C_2
$$

At the free surface,  $\tau(\delta) = \mu \frac{dw}{dx} = 0$ , or  $\frac{dw}{dx}\Big|_{x=\delta} = 0$ , hence  $C_1 = -\rho g \delta / \mu$ 

At the wall,  $w(0) = 0 = C_2$ 

Therefore

$$
w = \frac{\rho g}{2\mu} x^2 - \frac{\rho g \delta}{\mu} x = \frac{\rho g}{2\mu} (x^2 - 2\delta x)
$$
 (+4.5 points)

Part B:

(a) Maximum velocity is where  $\frac{dw}{dx} = \frac{\rho g}{2\mu}(2x - 2\delta) = 0$  or  $x = \delta$ , thus

$$
w_{max} = w(\delta) = -\frac{\rho g \delta^2}{2\mu} = -\frac{(891)(9.81)(0.002)^2}{(2)(0.29)} = -0.06 \, \text{m/s} \tag{+0.5 \, \text{point}}
$$

(b) Flow rate is

$$
Q = \int_0^{\delta} w(x) \cdot (-Wdx) = -W \cdot \left[ \frac{\rho g}{2\mu} \left( \frac{x^3}{3} - \delta x^2 \right) \right]_0^{\delta} = \frac{\rho g \delta^3 W}{3\mu}
$$
  
 
$$
\therefore Q = \frac{(891)(9.81)(0.002)^3(1)}{(3)(0.29)} = 8.04 \times 10^{-5} m^3 / s
$$
 (+0.5 point)

(c) Average velocity is

$$
\overline{w} = \frac{Q}{A} = \frac{Q}{W \cdot \delta} = \frac{8.04 \times 10^{-5}}{(1)(0.002)} = 0.04 \, \text{m/s}
$$
 (+0.5 point)

(d) Wall shear stress is

$$
\tau_{w} = \mu \frac{dw}{dx} \Big|_{x=0} = \mu \cdot \frac{\rho g}{2\mu} (2x - 2\delta) \Big|_{x=0} = -\rho g \delta = -(891)(9.81)(0.002) = -17.48 \, N/m^2
$$

(+0.5 point)

(e) Friction drag is

$$
D = \tau_w \cdot S = \tau \cdot (W \cdot H) = (-17.48)(1)(2) = -35 N \tag{+0.5 point}
$$